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# Decay-protected superconducting qubit with fast control enabled by integrated on-chip filters

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Achieving fast gates and long coherence times for superconducting qubits presents challenges, typically requiring either a stronger coupling of the drive line or an excessively strong microwave signal to the qubit. To address this, we introduce on-chip filters of the qubit drive exhibiting a stopband at the qubit frequency, thus enabling long coherence times and strong coupling at the subharmonic frequency, facilitating fast single-qubit gates, and reduced thermal load. The filters exhibit an extrinsic relaxation time of a few seconds while enabling sub-10-ns gates with subharmonic control. Here we show up to 200-fold improvement in the measured relaxation time at the stopband. Furthermore, we implement subharmonic driving of Rabi oscillations with a  $\pi$  pulse duration of 12 ns. Our demonstration of on-chip filters and efficient subharmonic driving in a two-dimensional quantum processor paves the way for a scalable qubit architecture with reduced thermal load and noise from the control line.

The physical realization of a universal useful quantum computer comes with very stringent technical requirements, including those summarized in the DiVincenzo criteria<sup>1</sup>. One such requirement is a high coherence-time-to-gate-time (CT2GT) ratio, ensuring that the physical system representing a quantum bit, qubit, stores the encoded information with high fidelity until the execution of the assigned task. This property is reflected in the measured energy relaxation time of the qubit,  $T_1$ , which is the time scale for the qubit to exponentially lose an excitation and return to its ground state. Various qubit modalities such as trapped ions<sup>2–5</sup>, spin qubits<sup>6–9</sup>, photonic qubits<sup>10–13</sup>, and superconducting qubits<sup>14–17</sup> are being explored for longer relaxation times to enhance the CT2GT ratio.

Superconducting qubits, in particular, have exhibited significant progress, with relaxation times extending from a few nanoseconds<sup>14,18–22</sup> to nearly a few milliseconds<sup>23–26</sup> over the past two decades. The quest for further improvement of the coherence time is still ongoing. Alternatively, gates can be sped up to further improve the CT2GT ratio<sup>27,28</sup>. However, this requires strong external coupling of the qubit to the drive line, which inadvertently decreases the coherence of the qubit, thereby posing a significant trade-off.

The coherence times of a qubit are influenced not only by the external coupling but also by intrinsic losses, which, in properly designed qubits, represent the primary loss mechanism, thus limiting the qubit performance. These losses arise from various sources, such as the presence of two-level-system defects near the qubit<sup>29–36</sup> associated with dielectric losses and quasiparticle tunneling<sup>37–40</sup>. Significant progress has been made in understanding<sup>41–49</sup> and mitigating these internal losses through the implementation of high-coherence materials<sup>25,26,50–53</sup>, fabrication recipes<sup>23,24,54,55</sup>,

and improved qubit geometry<sup>56,57</sup> leading to a situation where the external coupling should be made very weak not to limit qubit coherence, thus calling for high drive power at the qubit.

While engineering's very weak coupling to the qubit can increase the CT2GT ratio, it will impose a significant heat load on the dilution refrigerators that house the qubit, and especially on the attenuators that provide an electromagnetic environment for the qubit. To minimize the corresponding thermal noise reaching the qubit, attenuators are placed at multiple stages of the dilution refrigerators<sup>58</sup>. Additionally, this will also limit the number of gate operations that can be carried out before the cooling capacity of the dilution refrigerator is exceeded.

Recent progress<sup>59,60</sup> has shown promise in addressing the above-discussed challenge of simultaneously achieving fast control and long coherence time. However, the approach of ref. 59 raises concerns about quasiparticle generation due to the saturation of the Josephson junction employed in the qubit drive line at high power levels. Another important work<sup>60</sup> utilizes a novel way to drive a three-dimensional (3D) transmon qubit by subharmonics of the qubit resonance. Namely, the non-linearity of the qubit up-converts the drive at one-third of the qubit frequency to the qubit frequency in the spirit of three-wave mixing<sup>60</sup>. Inconveniently for scaling, the previous work employs bulky low-pass filters in the control line to suppress the spontaneous qubit decay to the strongly coupled drive line. Furthermore, to enable subharmonic control, only 43 dB of attenuation is used in the control line, which leads to a significant thermal noise photon of around 0.145 at a qubit frequency of 5 GHz.

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In this work, we introduce designs and provide implementations of on-chip filters for subharmonic driving in two-dimensional qubit schemes. The on-chip filters are devised to fully isolate the qubit from the drive line at its resonance frequency while establishing two orders of magnitude stronger coupling at the subharmonic frequency compared to standard drive lines. This result enables fast single-qubit gates via subharmonic drive while demonstrating the  $T_1$  limit owing to the external coupling of seconds, thereby substantially improving the corresponding CT2GT ratio. Encouragingly, the introduced on-chip filters facilitate the use of over 60 dB of attenuation in the control lines to ensure a thermal noise photon below  $2.5 \times 10^{-3}$ . Furthermore, we show that the use of a bulky low-pass filter creates unwanted resonances in the qubit drive line, modulating the measured  $T_1$  in extreme ranges. Thus our demonstration of subharmonic driving of a qubit in two dimensions, integrated with an on-chip filter, seems a promising pathway for scalable superconducting quantum processing units.

## Results

### Design and implementation of on-chip filters

We have developed two distinct versions of on-chip filters:  $\lambda/4$  and  $\lambda/2$  filters as shown in Fig. 1a, b. Essentially, these filters are coplanar-waveguide (CPW) transmission lines that connect capacitively to the qubit at the position  $x = 0$  and end in an open circuit at  $x = L_f$ , where  $L_f$  is the length of the filter. In the case of the  $\lambda/4$  filter,  $L_f = \lambda_q/4$ , where  $\lambda_q$  is the wavelength of the mode in the drive line at the qubit frequency. Similarly, for the  $\lambda/2$  filter,  $L_f = \lambda_q/2$ . We also note that  $\lambda/2$  filter couples to the qubit at two separate positions as opposed to the single-point coupling in the case of the  $\lambda/4$  filter. This two-point coupling design is inspired from multi-point coupling investigated in waveguide quantum electrodynamics<sup>61,62</sup>.

The working principle of the on-chip filters is illustrated in Fig. 1c, d. In the  $\lambda/4$  filter, the open-end creates a boundary condition for the voltage along the transmission line, resulting in a voltage anti-node at the open-end and a node at the qubit location when operating at the resonance frequency of the qubit as depicted in Fig. 1c. In contrast, the  $\lambda/2$  filter exhibits a voltage anti-node at both the  $x = 0$  and  $x = \lambda/2$  locations, but with opposite polarities as shown in Fig. 1d. Both configurations enforce net-zero voltage amplitude for the qubit, effectively decoupling the qubit from the drive line at the qubit resonance frequency. However, at the subharmonic frequency, the voltage

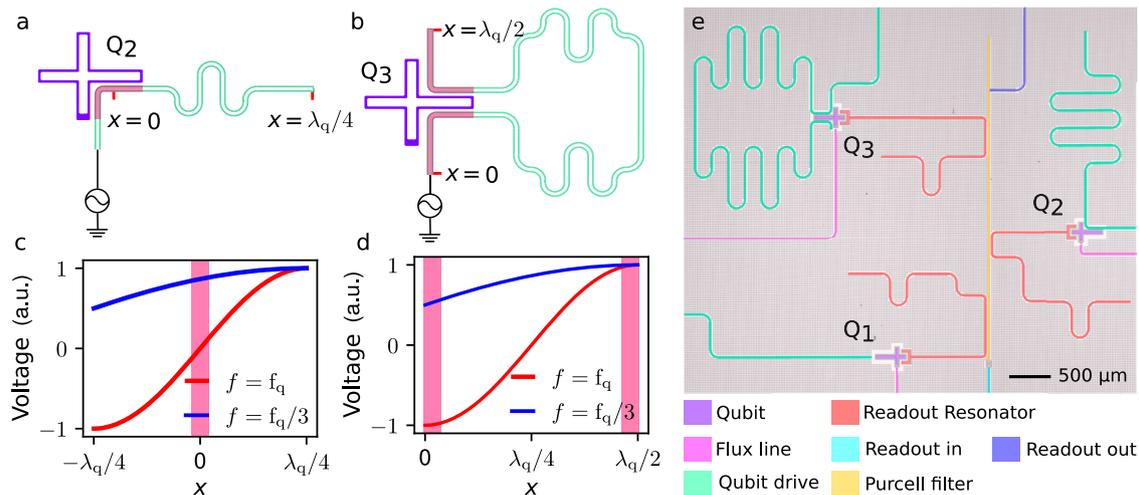
profile at the qubit is close to its maximum, thereby establishing a strong coupling between the qubit and the drive line. The length, over which the mode voltage is integrated to obtain the effective coupling strength between the mode and the qubit, is highlighted in Fig. 1a–d.

Our realized device is shown in Fig. 1e. The on-chip filters are integrated as a part of the qubit drive line. The device features three flux-tunable Xmon-style transmon qubits, labeled Q1, Q2, and Q3<sup>63</sup>. Qubit Q1 is connected to a standard, weakly coupled CPW transmission line. In contrast, qubits Q2 and Q3 are connected to  $\lambda/4$  and  $\lambda/2$  filters, respectively. Additionally, the device includes flux lines to tune the frequencies of the qubits. Each qubit is coupled to its respective quarter-wavelength resonator for readout. These readout resonators are inductively and capacitively connected to a common quarter-wavelength Purcell filter<sup>64</sup> to suppress qubit decay through the resonator.

We target the length of the on-chip filters such that their stopband is centered  $\sim 5$  GHz. The results of our numerical simulations of these filters are shown in Fig. 2. For a detailed description of the electromagnetic (EM) simulations, we refer to the Supplementary Note S1 in Supplementary Information.

Figure 2a,b depict a schematic and its equivalent lumped-element model of a qubit coupled to an on-chip filter and to a readout resonator. In the model, 50- $\Omega$  lumped ports, labeled P1 for the drive line, P2 for the qubit, and P3 for the readout resonator, are introduced for EM simulations. We focus on the scattering parameter  $S_{21}$ , which relates to the power transmission from the drive line to the qubit port, and on the input admittance  $Y_{in}$  parallel to the qubit. Here, we are only interested in the coupling between the drive line and the qubit. Therefore, both  $S_{21}$  and  $Y_{in}$  are calculated for the drive line port P1 matched to an impedance of 50  $\Omega$  and the resonator port P3 grounded. With this procedure, one can estimate the external coupling rate just from the drive line to be  $\gamma_q(\omega) = \text{Re}[Y_{in}(\omega)]/C_q$ <sup>65,66</sup>. In the low-temperature limit, the relaxation time is given by  $T_1(\omega) = [1/T_{1,\text{ext}}(\omega) + 1/T_{1,\text{diel}}(\omega) + 1/T_{1,\text{oth}}(\omega)]^{-1}$ , where  $T_{1,\text{ext}}(\omega) = 1/\gamma_q(\omega)$  is the contribution from just the external coupling to the drive line,  $T_{1,\text{diel}}(\omega)$  corresponds to the dielectric losses of the qubit, and  $T_{1,\text{oth}}(\omega)$  accounts for other sources of relaxation such as readout resonators, flux lines, etc.

Figure 2c shows that within the filter stopband centered at 5 GHz, the transmission from the qubit port to the transmission line lies



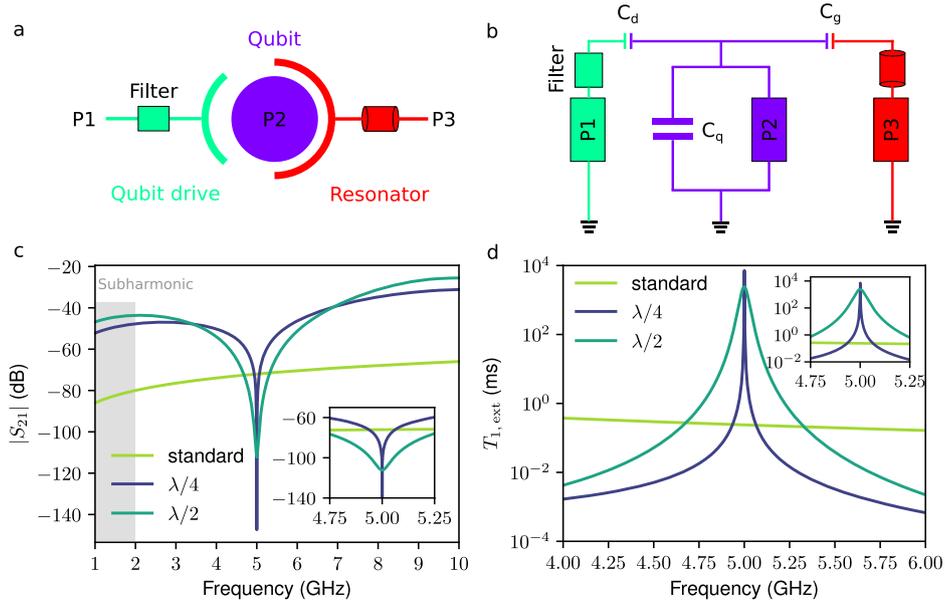
**Fig. 1 | Device layout with integrated on-chip filters.** a, b Schematic representation of qubits (white crosses) strongly coupled to a transmission line (turquoise) implemented as (a)  $\lambda/4$  and (b)  $\lambda/2$  filters at the qubit frequency  $f_q$  which corresponds to the full wavelength  $\lambda_q$ . c, d Voltage amplitude of the transmission line mode as a function of position  $x$  along the transmission line for the (c)  $\lambda/4$  and (d)  $\lambda/2$  filters. At the resonance frequency  $f = f_q$  (red line), both on-chip filters effectively decouple from the qubit due to net zero voltage at the qubit, whereas at the subharmonic frequency  $f = f_{q/3}$  (blue line), the on-chip filters couple strongly to the

qubit. The pink shading highlights the region where the modes couple to the qubit. e False-color optical-microscope image of the device. The device consists of three flux-tunable transmon qubits (violet) labeled Q1, Q2, and Q3. Each qubit is individually coupled to its own readout resonator (red) and flux lines (magenta). The readout resonators are further coupled to a common Purcell filter (yellow) for qubit readout. Additionally, qubits Q2 and Q3 are coupled to  $\lambda/4$  and  $\lambda/2$  filters respectively, whereas qubit Q1 is weakly coupled to a standard transmission line for control (turquoise).

below  $-110$  dB, greatly suppressed from  $-72$  dB obtained for the standard drive line. Importantly, within the subharmonic frequency range of  $1-2$  GHz, we observe an increase of over  $30$  dB in the transmission of the on-chip filters over the standard case.

In Fig. 2d, we examine the relaxation time  $T_{1,\text{ext}}$  of the qubit resulting from the external coupling to the drive line. Within the filter stopband, we observe an enhancement in  $T_{1,\text{ext}}$  by a factor of over  $1000$

with the  $\lambda/4$  and  $\lambda/2$  filters compared with the standard drive line. The estimated  $T_{1,\text{ext}}$  times at  $5$  GHz are as follows:  $0.3$  ms for the standard drive,  $7161$  ms for  $\lambda/4$  filter, and  $2421$  ms for  $\lambda/2$  filter. The widths of the frequency range where qubit  $T_{1,\text{ext}}$  exceeds  $1$  ms are  $70$  MHz and  $450$  MHz for  $\lambda/4$  and  $\lambda/2$  filter, respectively. We attribute this difference of feasible frequency ranges to the fact that the  $\lambda/2$  filter is of higher order than the  $\lambda/4$  filter since the coupling points of the qubit are located at the



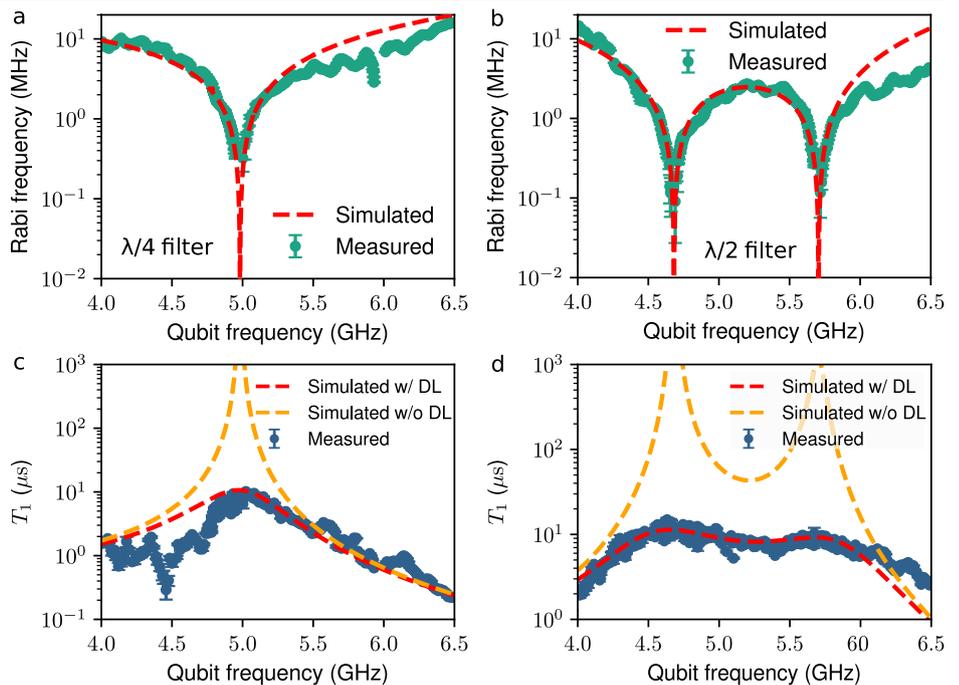
**Fig. 2 | Simulated transmission and relaxation time of the qubit from drive lines.**

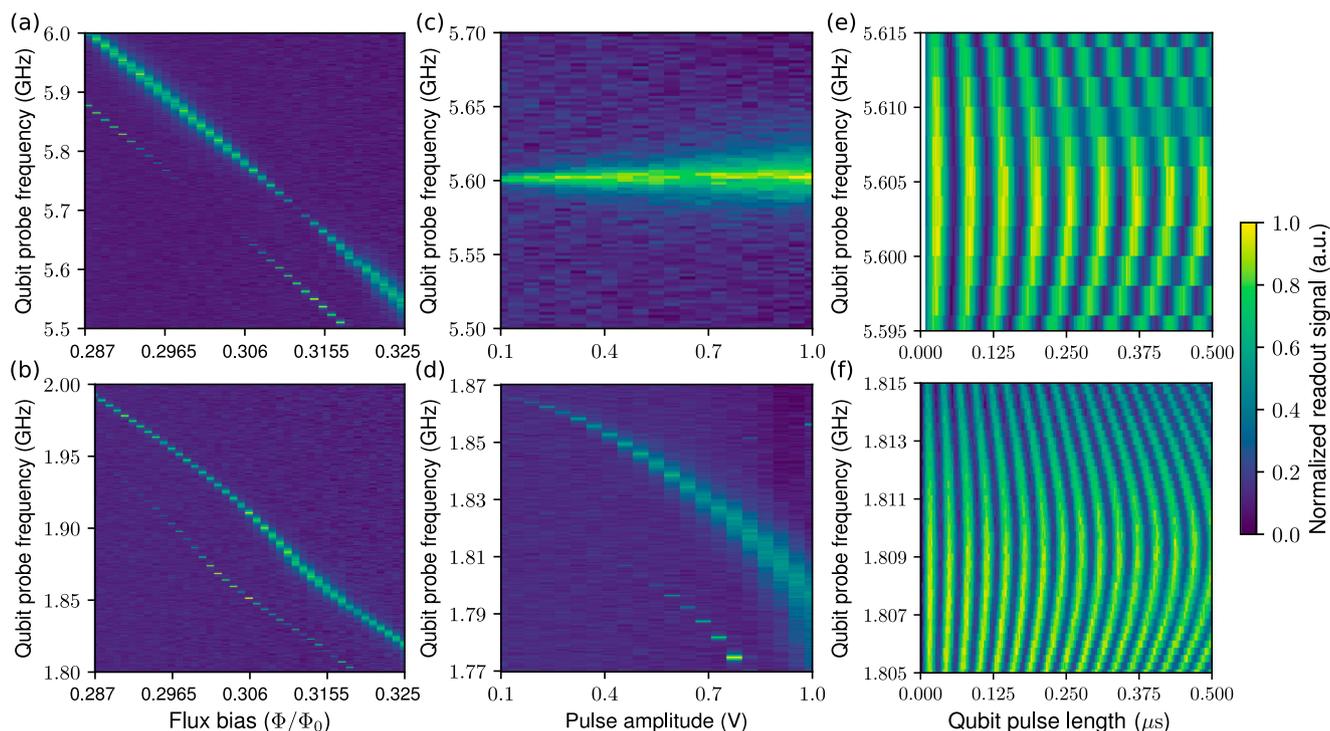
**a** Schematic of a 3-port network labeled P1, P2, and P3. Port P1 is connected to a qubit drive line through a filter which is a standard transmission line for Q1,  $\lambda/4$  filter for Q2, and  $\lambda/2$  filter for Q3. **b** Equivalent lumped-element model, where  $C_d$  is the capacitance between the qubit and the drive line,  $C_g$  is the capacitance between the qubit and the readout resonator, and  $C_q$  is the shunt capacitance of the qubit to the ground. The coupling capacitances  $C_d$  are  $80$  aF,  $4.5$  fF, and  $9.2$  fF for qubits Q1, Q2, and Q3, respectively. **c** Transmission amplitude from the qubit port to the drive line,  $S_{21}$ , as a function of frequency for the different filter configurations as indicated. The

$\lambda/4$  and  $\lambda/2$  filters are designed to have a stopband at  $5$  GHz. The inset highlights the region in the vicinity of the filter stopband for convenient comparison. The shaded gray region corresponds to transmission at subharmonic frequency. **d** Estimated relaxation time,  $T_{1,\text{ext}}$ , of the qubit owing to its coupling just to the drive line as a function of qubit frequency. This estimation is based on the total capacitance of the qubit and the input admittance  $Y_{\text{in}}$  parallel to the qubit port P2. At the stopband, the estimated relaxation times of the qubit for the standard drive, the  $\lambda/4$  filter, and for the  $\lambda/2$  filter are approximately  $0.3$  ms,  $7161$  ms, and  $2421$  ms, respectively.

**Fig. 3 | Characterization of the on-chip filters.**

**a, b** Measured (dots) and simulated (dashed line) Rabi frequencies of the qubit for (a)  $\lambda/4$  and (b)  $\lambda/2$  filters as functions of the qubit frequency  $f_q = \omega_q / (2\pi)$ . We swept qubit frequency in the range of  $4$  to  $6.5$  GHz and carried out the Rabi measurement to characterize the coupling strength of the drive lines to the qubit. The dashed line represents the Rabi frequency estimated using  $f_R = \Omega_R / 2\pi = 2\sqrt{\gamma_q}\beta$ , where  $\gamma_q = \text{Re}[Y_{\text{in}}] / C_q$  and  $\beta \propto \omega_q^{1/2} V$ , where  $V$  is the peak-to-peak voltage amplitude at the chip level. Note that the measured Rabi frequency for the  $\lambda/2$  filter shows two distinct stopbands centered around  $4.7$  GHz and  $5.7$  GHz, the presence of which is attributed to the unequal coupling at positions  $x = 0$  and  $x = \lambda/2$ . **c, d** Measured (dots) and simulated (dashed line) relaxation time,  $T_1$ , of the qubit for (c)  $\lambda/4$  and (d)  $\lambda/2$  filters as functions of the qubit frequency. The dielectric loss tangent of  $3 \times 10^{-6}$  obtained from the fit is used to account for dielectric losses limiting the  $T_1$ , represented by the red dashed line. While orange dashed line corresponds to the case without the dielectric losses. The simulated  $T_1$  also takes Purcell decay through the resonator into account. The error bars represent  $1\sigma$  fitting uncertainty.





**Fig. 4 | Spectroscopy and Rabi oscillations of qubit Q3 with resonant driving and subharmonic driving through the  $\lambda/2$  filter. a, b** Normalized readout signal of the qubit as a function of the flux bias and the frequency of the (a) resonant drive and (b) subharmonic drive. The top diagonal feature indicates the lowest transition frequency of the qubit and the bottom feature reveals the two-photon transition to the second excited state of the qubit. **c, d** Normalized readout signal of the qubit as a function of the driving-voltage amplitude at room temperature and the frequency of

the (c) resonant drive and (d) subharmonic drive for a flux bias of  $0.32 \Phi_0$ . Note the power broadening and up to  $-70$  MHz alternating-current (AC) Stark shift in (d) with increasing pulse amplitude. **e, f** Normalized readout signal of the qubit as a function of the pulse length and the frequency of the (e) resonant drive and (f) subharmonic drive for a flux bias of  $0.32 \Phi_0$ . In **e**, the pulse amplitude  $1$  V yields a Rabi frequency of  $17.57$  MHz and in **f**, we have  $0.9$  V and  $31.12$  MHz, respectively, at the Stark-shifted frequency of  $1.809$  GHz.

voltage anti-nodes where the gradient of the voltage with respect to position vanishes.

Assuming a coupling that results in  $T_{1,\text{ext}} = 1$  ms for a qubit driven resonantly through a standard transmission line, we estimate that a microwave pulse with a peak power of  $-11$  dBm at room temperature is necessary to implement  $10$ -ns single-qubit gates. With the above-simulated parameters of the on-chip filters, corresponding peak powers of  $-16$  dBm and  $-22$  dBm will be required for  $\lambda/4$  filter and  $\lambda/2$  filter, respectively, using a subharmonic drive approach. Thus the filters combined with subharmonic driving may yield a significant reduction in power consumption for single-qubit gates. These values are calculated considering  $60$  dB of attenuation in the drive line and a simple rectangular pulse shape. Note that the peak powers may significantly increase for complex pulse shapes, which are currently being used to minimize the leakage out of the computational subspace for high-fidelity gates<sup>37</sup>.

Furthermore, with the above estimates, we obtain a heat dissipation of  $-53$  dBm at the base plate resulting from a resonant drive with the standard transmission line. In the case of a subharmonic drive with the on-chip filters, we estimate heat dissipations of  $-58$  dBm with  $\lambda/4$  filter and  $-64$  dBm with  $\lambda/2$  filters.

### Characterization of on-chip filters

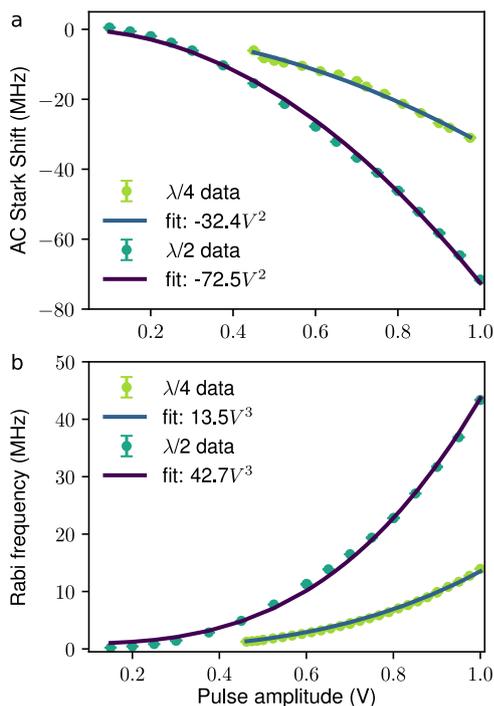
We follow the typical steps to fabricate the device on a silicon wafer, which includes a niobium metallization layer on top. The micron-sized features in the niobium are created using maskless lithography and etching, while the Manhattan-style Josephson junctions are patterned using electron-beam lithography and thermal evaporation of aluminum. We cool down the device in a commercial Bluefors XLD500 dilution refrigerator for cryogenic measurements. For more detailed information on the fabrication process

and the experimental setup, see the Supplementary Note S2 and S3 in Supplementary Information.

We carry out typical time-domain measurements to characterize the device parameters summarized in Table S1 in Supplementary Information. To quantify the performance of the on-chip filters, we measured the Rabi frequency and the  $T_1$  of the qubit around the target filter frequency of  $5$  GHz. A comprehensive description of the measurement sequence can be found in greater detail in the Supplementary Note S4 in Supplementary Information.

Figure 3a, b show the measured Rabi frequency for qubits driven through the  $\lambda/4$  and  $\lambda/2$  filters. We observe an impressive  $50$ -fold and  $220$ -fold suppression in measured Rabi frequency at the stopbands of  $\lambda/4$  and  $\lambda/2$  filters, respectively, corresponding to  $34$  dB and  $47$  dB changes in  $S_{21}$ . The suppression factor is defined with respect to the maximum Rabi frequency observed in the qubit frequency range of  $4$ – $6.5$  GHz. The simulated data depicted in Fig. 3a, b correspond to the Rabi frequency derived from the input admittance  $Y_{\text{in}}$  obtained through EM simulations, see Methods. Evidently, the measured and simulated Rabi frequencies exhibit a high level of agreement. Some minor deviations observed can be attributed to parasitic resonance and imperfections stemming from coupling with the control lines.

Note the significant discrepancy in the measured Rabi frequency for the  $\lambda/2$  filter shown in Fig. 3b in comparison to the simulated transmission depicted in Fig. 2c. In contrast to a single stopband at  $5$  GHz, we observe two stopbands centered around  $4.7$  GHz and  $5.7$  GHz. As detailed in Supplementary Note S1 in Supplementary Information, this splitting of the stopband mainly arises from the asymmetry in the coupling capacitance between the drive line and the qubit at the positions  $x = 0$  and  $x = \lambda/2$ , in addition to the fact that the coupling region at  $x = \lambda/2$  is of finite length. Consequently,



**Fig. 5 | Stark shifts and Rabi frequencies in subharmonic driving of qubits Q2 and Q3. a, b** Measured (markers) and model-fitted (solid lines) (a) AC Stark shift and (b) Rabi frequency for subharmonic driving through the  $\lambda/4$  and  $\lambda/2$  filters as indicated as functions of the voltage amplitude of the drive pulse at room temperature. The error bars indicate  $1\sigma$  uncertainty.

we show a good agreement between the measured and simulated results in Fig. 3b by introducing an asymmetric coupling at the open end of the  $\lambda/2$  filter in the EM simulation.

Figure 3c, d depict the measured  $T_1$  for the  $\lambda/4$  and  $\lambda/2$  filter. In our device, we consistently observe a  $T_1$  ceiling of approximately 10  $\mu$ s across all qubits. To investigate the reason for this limited  $T_1$ , we fit the Purcell decay and dielectric-loss models to the measured  $T_1$  of qubit Q1 near its readout resonator frequency, see Supplementary Note S5 in Supplementary Information. From the fit, we obtain a dielectric loss tangent of  $3 \times 10^{-6}$ , confirming dielectric loss as the primary loss mechanism in our device. Consequently, we used the dielectric loss tangent of  $3 \times 10^{-6}$  in the EM simulations, yielding the simulation results for qubits Q2 and Q3 in good agreement with the experiments. Without considering dielectric losses in the simulation, the extrapolated  $T_1$  at the filter frequency reaches hundreds of milliseconds range. Due to the Purcell decay through the resonator, the simulated  $T_1$  at the second stopband centered  $\sim 5.7$  GHz shows only a few milliseconds.

For the qubit  $T_1$  measured at the stopband of the filter, we observed a remarkable 20-fold improvement for the  $\lambda/4$  filter and an even more substantial 200-fold improvement for the  $\lambda/2$  filter in comparison to the values measured at the flux sweet-spot of the qubit, see Supplementary Table S1 in Supplementary Information. This enhancement has the potential for further improvements through the use of low-loss dielectric materials and implementation of state-of-the-art fabrication processes for high coherence.

### Resonant and subharmonic drive

Figure 4a, b present the flux spectroscopy results for qubit Q3 coupled to  $\lambda/2$  filter using both resonant and subharmonic driving techniques. By sweeping the flux bias  $\Phi$  threading through the SQUID in the units of flux quanta  $\Phi_0$ , we tune the frequency of qubit Q3 in a range of 500 MHz near the second stopband of the  $\lambda/2$  filter centered around 5.7 GHz. With resonant driving, we observe a major reduction in the qubit linewidth as it approaches the stopband at 5.7 GHz. Note that also the two-photon process to excite the

qubit from its ground state to the second excited state is visible at different flux bias but frequency matching to 5.7 GHz, consistent with the filter protecting the qubit at its stopband rather than the qubit itself being substantially different at a certain flux bias. However, with subharmonic driving, we observe a broadened qubit linewidth at around  $f = 5.7/3 = 1.9$  GHz. This observation indicates that the  $\lambda/2$  filter exhibits strong coupling at the subharmonic frequency but very weak coupling at the resonance frequency, which agrees with our intended design and purpose.

Qubit power spectroscopy with resonant driving in Fig. 4c demonstrates a broadening of the qubit line with increasing pulse amplitude. The spectroscopic line remains centered at the frequency of 5.6 GHz independent of the pulse amplitude. In contrast, Fig. 4d exhibits a pronounced AC Stark shift caused by the off-resonant nature of the subharmonic drive. The AC Stark shift of the qubit frequency is typical for an off-resonant driving of the qubit<sup>49</sup>. This shift increases with increasing pulse amplitude, reaching  $\sim 70$  MHz at the maximum amplitude used. The negative direction of the shift arises from the negative anharmonicity of the transmon qubit. Figure 4e, f illustrate Rabi oscillations of the qubit under resonant and subharmonic driving. For room-temperature pulse amplitudes of 1 V and 0.9 V, the measured Rabi frequencies for resonant and subharmonic driving are 17.57 MHz and 31.12 MHz, respectively. In the case of subharmonic drive, the Rabi frequency corresponding to the slowest oscillation occurs with an AC Stark shift of  $-57.67$  MHz.

### Rabi frequency and AC Stark shift

Figure 5a shows the AC Stark shift arising from the off-resonant nature of the subharmonic drive. For a maximum pulse amplitude of 1 V, the measured shift is  $\sim -33$  MHz for the  $\lambda/4$  filter and  $-73$  MHz for the  $\lambda/2$  filter. We obtain a good agreement between the measured Stark shift and the fit using a quadratic function in the pulse amplitude as theoretically expected from Eq. (5) in the “Method” section.

In Fig. 5b, we conduct a performance comparison between the  $\lambda/4$  and  $\lambda/2$  filters using the subharmonic drive. This comparison involves varying the pulse amplitude to measure the Rabi frequency at the AC-Stark-shifted frequency studied in Fig. 5a. We observe that the maximum measured Rabi frequency is approximately 13 MHz and 43 MHz, resulting in  $\pi$  pulses of lengths 37 ns and 12 ns with the  $\lambda/4$  and  $\lambda/2$  filters, respectively. We employ a cubic function to fit the measured Rabi frequencies as a function of the pulse amplitude, showing an excellent agreement with the experimental results as expected from the three-wave-mixing nature of subharmonic driving, as can be seen from Eq. (5) in the Method section. Importantly, we maintain over 70 dB of attenuation in the drive line to ensure that the thermal occupation of the qubit remains below 0.5%, and limit heat dissipation at the base plate to less than  $-40$  dBm = 100 nW.

### Discussion

In this work, we addressed the seemingly competing challenges of implementing fast single-qubit gates and mitigating the decoherence of qubits due to the strong coupling needed for such fast gates. These challenges are intimately related to the power dissipation budget in the dilution refrigerator that houses the qubits and cross-talk mitigation between the qubits.

A transmon qubit with a standard capacitive coupling to its broadband drive line resulting in  $T_{1,\text{ext}}$  of 1 ms requires a peak power of  $-11$  dBm at room temperature to implement 10-ns-long single-qubit gates using a resonant drive. This power requirement is estimated considering 60 dB attenuation in the drive line to keep thermal qubit excitations low. In contrast, a subharmonic drive requires roughly 25 dBm in this scenario with no drive line filter. Such drive power leads to heat dissipation of  $\sim -17.5$  dBm at the base plate, unfortunately matching its cooling capacity of  $-17$  dBm.

Our proposed on-chip filters are designed to achieve a  $T_{1,\text{ext}}$  bound of 7161 ms for the  $\lambda/4$  filter and 2421 ms for the  $\lambda/2$  filter at the stopband near the qubit transition frequency. We estimate peak powers of  $-16$  dBm for the  $\lambda/4$  filter and  $-22$  dBm for the  $\lambda/2$  filter at room temperature to implement 10-ns-long gates using subharmonic driving. With 60 dB of

attenuation in the drive lines, the heat dissipation at the base plate is reduced to  $-58$  dBm for the  $\lambda/4$  filter and to  $-64$  dBm for the  $\lambda/2$  filter, enabling tens of thousands of simultaneous gate operations before reaching the cooling power of typical refrigerators.

Experimentally, we achieved an impressive 50-fold and 220-fold suppression in the measured Rabi frequency and a factor of 50 and 80 improvements in the measured  $T_1$  at the stopbands of the  $\lambda/4$  and  $\lambda/2$  filters, respectively. We measured a maximum  $T_1$  of 10  $\mu$ s across the device, mainly limited by dielectric losses. The simulated and measured data exhibited excellent agreement, from which we conclude that the on-chip filters function as desired. We note that using state-of-the-art fabrication processes for high coherence and low-loss dielectric materials may further enhance these results and allow for more thorough study of the effects of the filters on the qubit energy relaxation time.

In our subharmonic-drive experiments, we obtained qubit spectroscopy akin to those with resonant driving using standard two-tone measurements. We measured  $\pi$  pulse lengths of 37 ns and 12 ns for the  $\lambda/4$  and  $\lambda/2$  filters, respectively, using Rabi measurements. This result was obtained with 62 dB of attenuation distributed across various dilution stages, combined with an additional 12 dB of attenuation from filters and wires at room temperature and inside the refrigerator, yielding  $\sim 74$  dB in total in the drive line. This configuration effectively reduced thermal noise photons to below  $2.5 \times 10^{-3}$  at qubit frequency and around 0.03 at subharmonic frequency. This is a prominent improvement compared to the work in ref. 60, where single-qubit gate of length 35 ns has been demonstrated with only 43 dB attenuation in the qubit control line and with the use of bulky off-chip low-pass filters.

The off-resonant nature of the subharmonic drive led to a substantial AC Stark shift of  $\sim -73$  MHz at a Rabi frequency of about 43 MHz with the  $\lambda/2$  filter, significantly more pronounced than in resonant driving. As a result, the standard approach for implementing and characterizing single-qubit gates through Randomized Benchmarking may not be feasible as such, calling for special attention to phase correction between gates. In addition, minimization of leakage errors with such brief gates is also pivotal. Although the drag scheme effectively reduces leakage errors in resonant driving, a similar approach adapted for subharmonic driving needs to consider the large AC Stark shift. Addressing this issue stands as an interesting topic for future research.

## Methods

### Single-qubit control

The Hamiltonian describing the control of the qubit has the following form

$$\hat{H} = \hat{H}_{\text{qubit}} + \hat{H}_{\text{drive}}(t), \quad (1)$$

where the first term on the right is the Hamiltonian of the undriven qubits and the second term is the drive Hamiltonian. The Hamiltonian of the transmon qubit is given by

$$\hat{H}_{\text{qubit}} = \hbar\omega_q \hat{b}^\dagger \hat{b} + \frac{\hbar\alpha}{2} \hat{b}^\dagger \hat{b}^\dagger \hat{b} \hat{b}, \quad (2)$$

where  $\omega_q$  is the angular frequency of the lowest qubit transition,  $\alpha$  is the anharmonicity, and  $\hat{b}$  and  $\hat{b}^\dagger$  are the annihilation and creation operators acting on the qubit states, respectively. The driving Hamiltonian assumes the form

$$\hat{H}_{\text{drive}}(t) = \hbar\Omega_R e^{-i\omega_d t - \varphi_d} \hat{b}^\dagger + \text{h.c.}, \quad (3)$$

where  $\Omega_R$  is the Rabi angular frequency, and  $\omega_d$  and  $\varphi_d$  are the frequency and the phase of the microwave drive. To implement arbitrary single-qubit gates, the Rabi frequency and the phase of the drive are temporally controlled.

In the case of resonant driving, we have  $\omega_d \approx \omega_q$ . By going into a frame rotating at  $\omega_d$ , we obtain a simplified qubit-drive Hamiltonian with the

detuning  $\delta_{\text{res}} = \omega_q - \omega_d$ ,

$$\hat{H}_{\text{res}} = \hbar\delta_{\text{res}} \hat{b}^\dagger \hat{b} + \frac{\hbar\alpha}{2} \hat{b}^\dagger \hat{b}^\dagger \hat{b} \hat{b} + \hbar(\Omega_R \hat{b}^\dagger + \text{h.c.}). \quad (4)$$

For the subharmonic driving, instead we have  $\omega_d = \omega_q/3 + \delta_{\text{sub}}$  and following the derivation in<sup>60</sup>, we find

$$\hat{H}_{\text{sub}} = \hbar(2\alpha|\eta|^2 - 3\delta_{\text{sub}})\hat{b}^\dagger \hat{b} + \frac{\hbar\alpha}{2} \hat{b}^\dagger \hat{b}^\dagger \hat{b} \hat{b} + \frac{\hbar\alpha}{3} (\eta^3 \hat{b}^\dagger + \text{h.c.}), \quad (5)$$

where  $\eta = \frac{\Omega_R(\omega_q - \alpha)}{\omega_d^2 - (\omega_q - \alpha)^2}$  represents the strength of the subharmonic drive.

From the Hamiltonian, we obtain the AC Stark shift  $\delta_{\text{sub}} = 2\alpha|\eta|^2/3$  resulting from the off-resonant drive and the subharmonic Rabi frequency  $\Omega_R^{\text{sub}} = 2\alpha|\eta|^3/3$ .

### Relation of the external coupling strength and Rabi frequency with admittance

In our experiments, we capacitively couple a CPW transmission line to the qubit for control. The interaction strength between the drive line and the qubit is given by ref. 67

$$\gamma_q = 2e^2 \left( \frac{C_d}{C_q} \right)^2 \left( \frac{E_J}{2E_C} \right)^{\frac{1}{2}} \frac{Z_{\text{tml}}\omega_q}{\hbar}, \quad (6)$$

where  $e$  is the elementary charge,  $C_d$  is the capacitance between the qubit and the drive line,  $E_J$  is the Josephson energy,  $E_C$  is the charging energy of the qubit,  $Z_{\text{tml}}$  is the characteristic impedance of the drive line, and  $C_q$  is the capacitance of the qubit island, respectively.

We express the Rabi frequency in terms of the interaction strength as

$$\Omega_R = 2\sqrt{\gamma_q}\beta, \quad (7)$$

where  $\beta = \left( \frac{1}{2\hbar\omega_q Z_{\text{tml}}} \right)^{\frac{1}{2}} V$  and  $V$  is the voltage amplitude of the drive<sup>67</sup>. From Eqs. (6) and (7), we observe that for the resonant case, the Rabi frequency  $\Omega_R \propto V$ , whereas for subharmonic drive,  $\Omega_R^{\text{sub}} \propto V^3$ . This cubic scaling with respect to the voltage amplitude renders the subharmonic drive favorable over resonant driving at high amplitudes or coupling strengths.

The above simplified analytical equation may be used to obtain  $\gamma_q$  of the qubit at weak coupling to the transmission line. In our case, we also consider the complete system of a qubit strongly coupled to an on-chip filter and to the readout resonator. Here, we resort to electromagnetic simulations to estimate the external coupling strength using  $\gamma_q(\omega) = \text{Re}[Y_{\text{in}}(\omega)]/C_q$ , where  $Y_{\text{in}}$  is the admittance in parallel with the qubit obtained from the simulations<sup>65,66</sup>.

### Electromagnetic simulations

The device layout is created using KQCircuits, an open-source Python library, within the KLayout editor. Subsequently, this layout is exported to the electromagnetic-simulation environment of the Sonnet software. Owing to the relatively large size of the qubit-drive geometry and the associated complexity of the simulation, we simplify the model by replacing a part of the transmission line by a lumped port, which allows for building a simulation of the full device using a lumped-circuit simulator.

The scattering-parameter data is exported from Sonnet to Microwave Office AWR, where we construct and simulate a full-circuit model. We extract and export the input admittance  $Y_{\text{in}}$  for further analysis in Python. A comprehensive description of the steps taken to achieve these simulation results is presented in the Supplementary Note S1 in Supplementary Information.

## Data availability

All relevant data and codes generating the figures in this article are available via Zenodo at <https://doi.org/10.5281/zenodo.11234842><sup>68</sup>.

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## Author contributions

A.S. and M.M. conceived the experiment. A.S. and S.K. designed and carried out the electromagnetic simulations of the device. H.S. and A.S. wrote the measurement codes for the experiment. Q.C. helped with the theoretical discussions on subharmonic drive. A.S. fabricated the device, conducted the experiments, and analyzed the results with feedback from S.K. A.S., S.K., and M.M. wrote the manuscript with comments from all the authors.

## Competing interests

M.M. declares that he is a Co-Founder and Shareholder of IQM Finland Oy. All other authors declare no competing interests.

## Additional information

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