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Chaperone-assisted translocation of flexible polymers in three dimensions

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Polymer translocation through a nanometer-scale pore assisted by chaperones binding to the polymer is a process encountered in vivo for proteins. Studying the relevant models by computer simulations is computationally demanding. Accordingly, previous studies are either for stiff polymers in three dimensions or flexible polymers in two dimensions. Here, we study chaperone-assisted translocation of flexible polymers in three dimensions using Langevin dynamics. We show that differences in binding mechanisms, more specifically, whether a chaperone can bind to a single site or multiple sites on the polymer, lead to substantial differences in translocation dynamics in three dimensions. We show that the single-binding mode leads to dynamics that is very much like that in the constant-force driven translocation and accordingly mainly determined by tension propagation on the cis side. We obtain $\beta \approx 1.26$ for the exponent for the scaling of the translocation time with polymer length. This fairly low value can be explained by the additional friction due to binding particles. The multiple-site binding leads to translocation the dynamics of which is mainly determined by the trans side. For this process we obtain $\beta \approx 1.36$. This value can be explained by our derivation of $\beta = 4/3$ for constant-bias translocation, where translocated polymer segments form a globule on the trans side. Our results pave the way for understanding and utilizing chaperone-assisted translocation where variations in microscopic details lead to rich variations in the emerging dynamics.

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I. INTRODUCTION

Polymer translocation through a nanopore has been a topic of major interest ever since Kasianowicz et al. suggested that the process could be used for inexpensive and fast DNA sequencing [1]. There is a plethora of studies to explain different aspects of the process in various circumstances. For a recent review, see [2].

Among different variants of polymer translocation, the process driven by binding particles (BiPs) has gotten less attention. In this form of polymer translocation, freely diffusing BiPs bind to the translocating polymer on the trans side. The bound BiPs block the polymer from reentering the pore and hence prevent its backwards motion towards the cis side. This Brownian ratcheting mechanism creates a bias to the polymer’s diffusion and drives the translocation.

An example in cell biology of a similar process is the protein translocation into the mitochondrial matrix [3–6]. It is believed that during the translocation auxiliary proteins called chaperones bind to the translocating polypeptide chain, which causes Brownian ratcheting.

The Brownian ratcheting was first theoretically studied in [7]. After this the topic has been discussed in a number of publications (see, e.g., [8–30]), some of which are computational studies. Monte Carlo simulations of the process have been reported in Refs. [12,20,21,24,25]. Extra care has to be taken to make sure Monte Carlo simulations capture the correct dynamics of translocation processes [31]. In this respect, Langevin dynamics (LD) simulations are a more straightforward approach [13,14,26,27,29,30]. Presumably due to the heavy computational requirements, the three-dimensional BiP driven translocation has not been much investigated by LD. The systems studied by LD are fairly small or in two dimensions. To our knowledge the only existing three-dimensional study concerns BiPs driving stiff chains [14], which does not capture the true dynamics of nonrigid polymers.

The motivation for studying binding-particle driven translocation of stiff polymers was to facilitate a theoretical basis for the more complicated case of flexible polymers [14]. It was argued that the essential features of the process would be covered by including the dynamics within the polymer’s persistence length from the pore. However, from the numerous studies of translocation driven by force applied at the pore we know that changes in the conformation of the nonrigid polymer during translocation largely determine the dynamics (see, e.g., [32–34]).

Flexible BiP driven polymers and the effect of flexibility have been studied in two dimensions [26,29,30]. With stiff polymers particle binding was unambiguous: BiPs can only bind to one site (polymer segment) at a time. Introducing flexibility changes this. In Refs. [26,29] BiPs were allowed to bind to multiple polymer segments simultaneously. However, in many known cases in cellular biology a protein has only a single binding site for interactions with another molecule. When this is the case, a binding model that restricts the binding of BiPs to only a single segment of the polymer at a time should be used.

Here, we investigate the BiP driven translocation of flexible polymers in three dimensions using Langevin dynamics. We apply two different binding models. In the one-to-one (OTO) binding model we restrict the binding of BiPs to only a single monomer at a time. In the all-to-all (ATA) binding model we allow BiPs to bind to all monomers in their vicinity. Regarding previous studies the OTO model introduces polymer flexibility to single site binding of stiff polymers, whereas the ATA model introduces the third dimension to the two-dimensional models studied in Refs. [26,30].
We show that the processes in three dimensions are crucially different from the processes in two dimensions and that changing the binding mechanism completely changes the process in three dimensions. We compare translocation driven by OTO binding to translocation driven by a constant pore force and show that also the dynamics of the OTO driven process is mainly determined by tension propagation in the polymer segment on the cis side. Close resemblance in the tension propagation of the BiP-assisted and pore force driven translocation was recently seen in two dimensions [30].

In what follows, we first outline the computational setting by describing models used for polymers, binding particles, dynamics, and the pore and the membrane. We then report and analyze the results from our simulations. Finally, we recap the main conclusions of our study.

II. THE COMPUTATIONAL MODELS

The three-dimensional simulation space consisting of a translocating polymer, binding particles (BiPs), membrane walls, and periodic boundaries is depicted in Fig. 1. In what follows cis and trans signify the sides of the membrane on which the polymer resides initially and to which it translocates, respectively.

A. The polymer model

Excluded volume interactions of the polymer are taken into account via a Lennard-Jones (L-J) potential acting between any two polymer beads (PBs):

\[
U_{LJ} = 4\epsilon \left[ \left( \frac{\sigma}{r} \right)^{12} - \left( \frac{\sigma}{r} \right)^{6} + \frac{1}{4} \right], \quad r \leq 2^{1/6} \sigma. \tag{1}
\]

Here, \( \epsilon = 1.0 \) is the strength of the interaction, \( \sigma = 1.0 \) is the length scale of the interaction, and \( r \) is the current distance between two PBs. By setting the cutoff distance \( r = 2^{1/6} \sigma \) to exclude attractive interactions we model the polymer to be immersed in good solvent.

The polymer is modeled as a freely jointed bead spring chain. Adjacent PBs are connected together by a finitely extensible nonlinear elastic potential:

\[
U_F = -K R^2 \ln \left( 1 - \frac{r^2}{R^2} \right), \tag{2}
\]

where \( K = \frac{20 \sigma^3}{V^2} \) is the strength of the attractive interaction, \( R = 1.5 \sigma \) is the maximum distance, and \( r \) is the current distance between two connected PBs.

B. The binding particle model

The interaction between any two BiPs is modeled with the repulsive L-J interaction of Eq. (1). A slightly different L-J potential is used for modeling the interaction between a BiP and a PB. First, a PB and a BiP can bind together via the attractive part of the L-J interaction. Second, we use \( \epsilon_b \) instead of \( \epsilon \) for the binding strength of the BiPs to the PBs. The BiP-PB interaction hence takes the form

\[
U_{LB} = 4\epsilon_b \left[ \left( \frac{\sigma}{r} \right)^{12} - \left( \frac{\sigma}{r} \right)^{6} + \frac{1}{4} \right], \quad r \leq r_{\text{max}}. \tag{3}
\]

The binding strength is chosen to be \( \epsilon_b = 8.0 \). Only when investigating the effect of the binding strength \( \epsilon_b \) is varied between 1.0 and 64.0.

The binding and unbinding are controlled via the threshold distance \( r_{\text{max}} \). We conduct our simulations with two different models for binding. In both models the binding is described by Eq. (3) and can only take place between a BiP and a PB. In the ATA binding model every BiP-PB pair can bind together when they are within the distance \( r_{\text{bind}} = 1.84 \sigma \) of each other. Equation (3) is hence used with \( r_{\text{max}} = r_{\text{bind}} \) for all BiP-PB pairs. This allows each BiP (PB) to bind to many PBs (BiPs) simultaneously. ATA hence corresponds to the intersegment binding model of \([26,29]\). In contrast, in the OTO binding model each BiP is allowed to bind to only one PB at a time. When an unbound BiP and an unbound PB are within \( r_{\text{bind}} \) of each other, a binding takes place and Eq. (3) is used with \( r_{\text{max}} = r_{\text{bind}} \). For any BiP (PB) interacting with an already bound PB (BiP), \( r_{\text{max}} = 21/6 \sigma \) and only the repulsive part is applied. A BiP-PB pair is considered broken if the BiP and PB get farther than \( r_{\text{bind}} \) apart.

For both models binding between a PB and a BiP can only occur if the PB has entered the trans side. This prevents binding of a BiP to a PB that is still inside the pore and, consequently, the BiP from pulling the PB from the pore to the trans side. If a bound PB reenters the pore, its binding to the BiP is not broken.

Since the binding and unbinding take place according to the distance of the BiP and the monomer to which it binds,
the stochastic nature of this process comes about via the stochastic motion of the particles. Adding explicit binding and unbinding rates would give more freedom in defining, e.g., highly asymmetrical binding and unbinding probabilities. This would, however, slow down the translocation process and make the simulation of the three-dimensional chaperone-assisted translocation computationally an overwhelming task. The binding and unbinding described here are used in the previous studies in two dimensions, which enables us to make direct comparisons to them.

C. The dynamics of polymer and BiPs

The dynamics for the pointlike PB and BiP particles is implemented using Ermak’s version of Langevin dynamics [35]. The Langevin equation governing the dynamics of a particle indexed $i$ is written as

$$\dot{p}_i = -\xi p_i + \eta_i(t) + f_i(r_i),$$

(4)

where $p_i$ is the momentum of the particle and $\dot{p}_i$ is its time derivative, $\xi$ is the friction coefficient of the implicit solvent, $\eta_i$ is the resultant random force exerted on the particle, $f_i(r_i)$ is the resultant force exerted on the particle, and $r_i$ is the position of the particle. The velocity Verlet algorithm is used to integrate the positions and velocities of the particles related by the Langevin equation [36].

Parameter values used in the simulations are given in reduced units. The Boltzmann constant $k_B = 1.0$ and the temperature $T = 1.0$. The time step $\delta t = 0.001$ and the friction coefficient $\xi = 0.5$ to which we also relate $\eta_i(t)$ according to the fluctuation dissipation theorem. The masses of both PBs and BiPs are $m = 16.0$.

D. The pore, membrane, and boundary conditions

The simulation space consists of two compartments separated by a membrane. The membrane is modeled by a wall of thickness $3\sigma$. Slip boundary conditions are applied for all beads colliding with the two wall surfaces. A circular pore of diameter $2\sigma$ penetrates the wall allowing PBs to pass from one side to the other. BiPs residing on the trans side cannot enter the pore.

The pore is implemented by a harmonic force that pulls the PBs toward an axis orthogonal to the wall surfaces:

$$f_h = -k_pr_p - cv_p.$$  

(5)

Here, $r_p$ is the distance of the PB from the pore axis and $v_p$ is the velocity of the PB perpendicular to the pore axis. The coefficient values were chosen as $k_p = 100.0$ and $c = 1.0$. In addition to the harmonic force aligning the polymer, hairpinning is prevented also by only allowing PBs to enter the pore sequentially.

Periodic boundaries in $x$ and $y$ directions and a slip wall perpendicular to the $z$ direction prevent the BiPs on the trans side from diffusing away. The periodic boundary conditions and the wall are applied for both PBs and BiPs. The slip wall in the $z$ direction is placed so far that only a few of the longest ($N = 400$) polymers under OTO binding touch the wall.

E. About the simulations

At the start of all simulations almost the entire polymer is on the cis side. A short segment is inside the pore and two monomers in the head protrude to the trans side. All the BiPs are on the trans side. See the first snapshot in Fig. 2.

Simulations are started from equilibrated polymer conformations. A polymer is equilibrated while keeping the polymer end fixed. During equilibration we measure the radius of gyration $R_g = \sum_{i=1}^{N}(r_i - r_{CM})^2$, where $r_{CM}$ is the polymer’s center of mass. An equilibrium conformation is considered to be reached when the time-averaged $R_g$ has converged to a stable value. After the polymer equilibration the BiPs on the trans side are also allowed to find an equilibrium distribution and bind to the two PBs on the trans side. After this the polymer is released, and translocation begins.

For all sets of presented data we have conducted 300 simulations. There are some exceptions: For polymers of length $N = 400$ with cis dynamics excluded, we conducted 100 simulations each. For simulations used to calculate the equilibrium $R_g$, 50 time-averaged simulations were used. It should also be noted that for small binding strengths $\epsilon_b$ a number of translocations do not complete due to some polymers sliding back to the cis side. In these cases the number of simulations can be considerably less than 300. For the
intermediate value $\epsilon_b = 8$ used in most of our simulations around 10% of the polymers do not translocate.

In the simulations we fix the concentration of free BiPs to $c_f = 1/40$ unless stated otherwise. The exceptions are simulations for investigating the effect of $c_f$. Here $c_f$ is chosen between 1/320 and 1/5. The value of $c_f$ is maintained by creating a new BiP at the edge of the simulation space if $c_f$ drops below a threshold value.

III. RESULTS

A. Different binding causes visible difference in translocation

The snapshots from the simulations in Fig. 2 show how the two different binding models affect translocation. They are taken from simulations conducted with polymers of length $N = 400$. The snapshots in the upper and lower rows are from single simulations using OTO and ATA, respectively. In OTO the polymer takes a diffuse conformation on the trans side, whereas ATA brings the polymer to a highly folded conformation consisting of helical regions (see Fig. 3). The strong folding markedly differs the translocation driven by ATA binding in three dimensions from the corresponding process in two dimensions. In two dimensions the intersegmental binding in ATA binding is much more restricted than in three dimensions, so the difference to translocation driven by OTO binding is not as significant in two dimensions as in three dimensions.

B. Relaxation of the polymer segment on the trans side

In our previous studies on driven polymer translocation we measured $R_g$ for segments on the trans side to determine if the translocation of segments was faster than relaxation of translocated segments to equilibrium. We found that translocated segments do not have time to relax but are driven increasingly further out of equilibrium as the number of translocated monomers $N_u$ increases. This shows as the difference $R_{gR}(N_u) - R_{gR}(N_u)$ increasing with $N_u$, where $R_{gR}(N_u)$ is the radius of gyration for an equilibrium conformation of a polymer of length $N_u$ [33,37].

C. Waiting times: Contribution of tension propagation

Waiting time $t_w(s)$ is the average time for the bead $s$ to exit the pore after the bead $s + 1$ has exited. Its measurement is the most straightforward way to gain understanding on translocation dynamics. We calculate waiting times by subtracting the last passage time of the current bead from that of the previous bead. We have checked that using first passage times instead does not change the waiting time profiles.

In order to assess the role of the cis side on the dynamics of the BiP driven translocation models we also simulate a modified model where the polymer beads on the cis side are excluded. In this modified model we do not have a polymer segment on the cis side but generate PBs at the pore entrance. Should the polymer slide back, the PBs entering the cis side are removed from the polymer. We have previously used this method in connection with the driven polymer translocation [37].

Figure 5 shows the ensemble averages of the waiting times $t_w(s)$ for the full (a) and modified (b) OTO model and for the full (c) and modified (d) ATA model. The waiting time data are
inherently noisy. The amount of statistics required to suppress the noise to an insignificant level would be unfeasible for the system sizes used here. Accordingly, the presented data have been slightly Gaussian filtered for improved clarity.

ATA binding induces stronger bias than OTO binding, so the waiting times for ATA are clearly shorter. Also the shapes of the waiting time profiles for ATA and OTO are clearly different.

Excluding the cis side dynamics has a dramatically different effect on ATA and OTO models. The waiting time profile for OTO becomes almost flat when the cis side is excluded, whereas the $t_w(s)$ for ATA change only mildly. The stronger binding on the trans side in the ATA model not only speeds up the translocation but also enhances the correlations along the polymer on the trans side, as seen in Figs. 2 and 3. Accordingly, in the ATA binding the friction for the movement of the polymer segment on the trans side is larger than in the OTO model. The trans side contribution is expected to be cis side is excluded, seen from the larger size and the darker shade of the area above the diagonal. Tension propagation in the two models is clearly similar. In the ATA model the tension propagation is slightly more prominent as seen from the larger size and the darker shade of the area above the diagonal.

By extracting contours for different values of the two-point distance we gain a more precise picture of the tension propagation in different models. The number of beads $n_d$ experiencing a certain magnitude of drag can be calculated by subtracting the diagonal value from the value of $i$ for each $s$. The outcome is depicted in Figs. 7(b) and 7(d). Shown are all two-bond distance values greater than the equilibrium value $l_d = 1.59$ for our self-avoiding polymer. The top curve $n_d(s)$ in each subfigure corresponds to the contour for the two-bond distance value of $l_d = 1.60$. The subsequent $n_d(s)$ curves are plotted for $l_d = 1.62,...,1.64$ up to a value where the corresponding contour can no longer be distinguished from the diagonal of the respective left column plots of Fig. 7. The higher the $l_d$ for the contours that can be distinguished, the more prominent is the tension propagation. Hence, it can be seen that tension propagation is most prominent in the ATA binding. This can be accounted for by the ATA binding leading to faster translocation.

To further assess how largely tension propagation defines the translocation dynamics in the case of OTO binding we compare the waiting times and tension propagation in
translocations driven by OTO and pore force. We have previously shown that the trans side has no discernible contribution on the dynamics in the case of driven translocation [37]. Hence, the translocation driven by pore force can be used as a reference for polymer translocation the dynamics of which is practically completely determined by tension propagation. Figures 8(a) and 8(b) give the above-described tension propagation data for the driven polymer translocation. The pore force $f_d = 0.25$ was selected so that it takes the same average time for polymers of length $N = 400$ to complete the driven and the OTO translocation. Accordingly, the closest match of $t_{w}(s)$ is seen for $N = 400$.

Figure 9 compares OTO and $f_d$ driven translocation. Here, the extent of the tensed segment on the cis side in the number of beads in drag $n_d$ is shown in the left column, and the waiting times $t_{w}$ as functions of the number of translocated beads $s$ are shown in the right column for different $N$. The tension on the cis side is seen to propagate identically in translocations driven by pore force and OTO binding. There are minor differences in the waiting time profiles. As the frictional contribution due to tension propagation on the cis side is seen to be identical these differences have to come solely from the trans side where the binding changes the polymer conformation: the altered friction and inertia due to binding particles directly affect the translocation dynamics.

D. Bias due to binding

The bias driving the polymer through the pore is caused by two factors: energy drop on the trans side and Brownian ratcheting, both caused by the binding particles. For the completely stiff (rod) polymer it was found that the driving caused by the energy drop dominates over the perfect Brownian ratchet mechanism [14]. To determine the dominating mechanism in the case of a flexible polymer we simulate a three-dimensional translocation model where the polymer is driven by perfect ratchetting only. The model geometry is the same as in ATA-, OTO-, and $f_d$-driven models. There is no driving force nor binding particles; only the backward motion of the polymer segment inside the pore is completely inhibited to realize perfect ratcheting. Figures 8(c) and 8(d) show the tension propagation characteristics for perfect Brownian ratcheting. Tension propagation for the perfect Brownian ratchet is seen to be clearly the strongest of the different models.

In Fig. 10 $t_{w}(s)$ for the full models and ones where the cis side is excluded are given for the driven translocation and the perfect ratchet model. The perfect Brownian ratchet mechanism is seen to be clearly faster than the translocations driven by constant force and the binding particles (see Fig. 5). As seen in Fig. 10, eliminating the cis side in the Brownian ratchet dynamics results in a completely flat $t_{w}(s)$. For the full ratchet model $t_{w}(s)$ is identical in form to that of the driven translocation (see Fig. 10). This confirms that tension propagation on the cis side predominantly determines the dynamics in perfect Brownian ratcheting like in the driven translocation.

In the OTO model particle unbinding allows for some backward motion of the polymer, so the ratcheting mechanism is not perfect. Our simulations show that the model with
Brownian ratcheting alone without energy reduction due to binding gives by far the strongest bias of all the simulated modes. This suggests that it is the Brownian ratcheting that dominates in three dimensions the translocation of a flexible polymer by binding particles, not the reduction of the free energy on the trans side due to binding. This is in contrast to what was found for chaperone-assisted translocation of stiff polymers [14].

**E. Translocation time versus polymer length**

Here, we verify the above-presented analysis by looking at the scaling of translocation time $\tau$ with polymer length $N$ in the different model systems. Figure 11 shows average $\tau$ as a function of $N$ for the full and modified binding models. The error bars of the data points are much smaller than the used symbols. Figure 11 also shows the scaling relations $\tau \sim N^\beta$ fitted to the data. The scaling exponents are $\beta = 1.26 \pm 0.02$ and $1.09 \pm 0.01$ for the full OTO model and one where the polymer segment on the cis side is excluded, respectively. The corresponding exponents for the full and modified ATA models are $\beta = 1.36 \pm 0.01$ and $1.34 \pm 0.02$, respectively.

Removal of segments on the cis side reduces $\beta$ from 1.26 to 1.09 in the OTO binding. The drop of $\beta$ to almost 1 due to the linear scaling, confirms our observation that the trans side has only a minimal effect on the translocation driven by OTO binding and, consequently, the weak tension propagation on the cis side largely determines the dynamics. The fairly low value of $\beta = 1.26$ is understandable, since particles binding to the polymer in the vicinity of the pore increase the local friction there. This leads to reduced $\beta$ for polymers of modest length [33].

The obtained superlinear scaling with $\beta > 1$ due to the trans side could potentially come from crowding of the segment close to the pore. In the driven translocation the effect of the crowding was shown to be negligible. Inclusion of the trans side was nevertheless found essential as only then $\beta$ increased with $f_d$ [37]. This was addressed to fluctuations assisting translocation [39]. However, the driving bias due to chaperones is weaker and small perturbations on the trans side are expected to show more easily in the outcome. Moreover, unlike in $f_d$ driven translocation crowding may play a role in the BiP driven case, since BiPs increase the time it takes for the translocated segments to relax to thermal equilibrium. The binding rate may also slow down due to the diffusion of
and, as shown, comes mainly from the fd models. Translocation driven by the pore force \( \beta = \beta \) measured driving the polymer segment would be instantly drawn from the OTO, obtained by fitting the perfect ratchet no cis driven \( (d) \sim \langle R_g \rangle \sim s^{3/2} \). The mass of the packed globule on the trans side grows as \( m \sim s \), which leads to \( p \sim s v \) and, consequently, \( v \sim 1/s \). The time average over the whole translocation scales as \( v = v = 1/\tau \int_0^s v \, ds \sim 1/\tau \int_0^s v(s) \, ds \sim N^{-1} \). Accordingly, it can be taken as the effective velocity over the whole process, \( \langle v \rangle = \langle v_c \rangle \). The average translocation time, as \( s \to N \), then becomes \( \tau = \langle d \rangle / \langle v \rangle \sim N^{3/2} \).

In reality, the effective bias due to binding of course varies somewhat, due to which \( p \) does not remain strictly constant. Also \( R_g \) does not scale strictly spherically. Departure from these assumptions causes \( \beta \) to deviate from the predicted value \( \beta = 4/3 \). Still, the measured value \( \beta = 1.36 \) is very close.

In translocations driven by the perfect Brownian ratchet mechanism scaling relations for the full model and one where polymer segments on the cis side are removed confirms that the dynamics is mainly determined by the tension propagation on the cis side [see Figs. 10(c) and 10(d)]. From Fig. 11(b) the scaling exponents \( \beta \) seen to be somewhat smaller than for the translocation driven by a constant pore force \( f_d \). \( R_g(s) \) on the trans side for the perfect ratchet model and translocation driven by \( f_d \) are almost identical (not shown), so based on our previous results \[37\] in spite of \( R_g(s) \) being smaller than the equilibrium \( R_g \), this crowding on the trans side has no effect on translocation dynamics.

As described, our perfect ratchet model does not involve any binding particles but ratcheting comes from not allowing the polymer to slide back toward cis. Hence, the only qualitative difference to constant-force-driven translocation is that fluctuations in reaction coordinate \( s \) are rectified. In other words, fluctuations that would move the polymer back toward cis are eliminated and only forward directed fluctuations are allowed. Hence, the assistance of the fluctuations in translocation is further enhanced compared to driven translocation \[39\], resulting in a smaller \( \beta \).

The measured value for \( \beta \) in ATA binding can be understood as follows. For the moment, we assume that the number of bindings close to the pore, which determines the driving force, is approximately constant. Based on our measurements of the binding and unbinding during translocation this is not far from the truth. Consequently, in this approximation the bias due to binding and hence the momentum in the direction of translocation \( p = p = m v \) are constant. Here, \( v = v \) is the (scalar) translocation velocity in the direction perpendicular to the wall and \( m \) is the moving mass. Due to the strong attraction between monomers where BiPs attach, we assume the average distance from the pore to which the center-of-mass point has been moved on the trans side to scale with the number of translocated monomers as the gyration radius of the expanding globular conformation \( \langle d \rangle \sim \langle R_g \rangle \sim s^{3/2} \). The mass of the packed globule on the trans side grows as \( m \sim s \), which leads to \( p \sim s v \) and, consequently, \( v \sim 1/s \). The time average over the whole translocation scales as \( v = v = 1/\tau \int_0^s v \, ds \sim 1/\tau \int_0^s v(s) \, ds \sim N^{-1} \). Accordingly, it can be taken as the effective velocity over the whole process, \( \langle v \rangle = \langle v_c \rangle \). The average translocation time, as \( s \to N \), then becomes \( \tau = \langle d \rangle / \langle v \rangle \sim N^{3/2} \).

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In reality, the effective bias due to binding of course varies somewhat, due to which \( p \) does not remain strictly constant. Also \( R_g \) does not scale strictly spherically. Departure from these assumptions causes \( \beta \) to deviate from the predicted value \( \beta = 4/3 \). Still, the measured value \( \beta = 1.36 \) is very close.

In translocations driven by the perfect Brownian ratchet mechanism scaling relations for the full model and one where polymer segments on the cis side are removed confirms that the dynamics is mainly determined by the tension propagation on the cis side [see Figs. 10(c) and 10(d)]. From Fig. 11(b) the scaling exponents \( \beta \) seen to be somewhat smaller than for the translocation driven by a constant pore force \( f_d \). \( R_g(s) \) on the trans side for the perfect ratchet model and translocation driven by \( f_d \) are almost identical (not shown), so based on our previous results \[37\] in spite of \( R_g(s) \) being smaller than the equilibrium \( R_g \), this crowding on the trans side has no effect on translocation dynamics.

As described, our perfect ratchet model does not involve any binding particles but ratcheting comes from not allowing the polymer to slide back toward cis. Hence, the only qualitative difference to constant-force-driven translocation is that fluctuations in reaction coordinate \( s \) are rectified. In other words, fluctuations that would move the polymer back toward cis are eliminated and only forward directed fluctuations are allowed. Hence, the assistance of the fluctuations in translocation is further enhanced compared to driven translocation \[39\], resulting in a smaller \( \beta \).

F. Concentration and binding force dependence of the translocation time

In previous sections the free BiP concentration and the binding constant were set at \( c_f = 1/40 \) and \( \epsilon_b = 8.0 \), respectively. Here we investigate how the translocation times are affected when \( c_f \) is varied between 1/320 and 1/5 and binding strength \( \epsilon_b \) between 1.0 and 64.0.

Figure 12 shows the average translocation times \( \tau \) as a function of \( c_f \). The simulations were done for \( N = 50 \) and


FIG. 11. Scaling of the translocation times. Scaling exponents obtained by fitting \( \tau \sim N^\beta \) to the data. (a) The BiP driven models. OTO, \( \beta = 1.26 \pm 0.02 \); ATA, \( \beta = 1.36 \pm 0.01 \); OTO no cis, \( \beta = 1.09 \pm 0.01 \); and ATA no cis, \( \beta = 1.34 \pm 0.02 \). (b) The reference models. Translocation driven by the pore force \( f_d = 0.25 \), \( \beta = 1.39 \pm 0.02 \); driven by the perfect Brownian ratchet mechanism, \( \beta = 1.32 \pm 0.01 \); driven \( f_d = 0.25 \) no cis, \( \beta = 1.08 \pm 0.02 \); and driven by the perfect ratchet no cis, \( \beta = 1.04 \pm 0.01 \).
that in three dimensions the differences in binding lead to substantial differences in translocation dynamics.

In the OTO binding the polymer is driven increasingly out of equilibrium much the same way as in the case of constant pore force \( f_d \) driving the translocating polymer. We showed that for this binding tension propagates on the cis side in exactly the same way as in \( f_d \)-driven translocation. In spite of this similarity waiting time profiles showed differences for the two cases. Translocation assisted by OTO binding is slightly slowed down compared to the \( f_d \)-driven case. Obviously, the differences have to come from the trans side. Crowding of the polymer segment, which we have previously shown not to affect \( f_d \)-driven translocation, can to some extent impede chaperone-assisted translocation, since the inertia and friction of the polymer segment on the trans side are increased due to binding particles.

The main conclusion concerning OTO-binding assisted translocation in three dimensions is that its dynamics is mainly determined by tension propagation on the cis side and that the tension propagates exactly like the tension in translocation driven by pore force the magnitude of which equals the bias due to binding chaperones. The exponent for scaling of the translocation time with the polymer length, \( \tau \sim N^{\beta} \), in OTO-binding assisted translocation was found to be \( \beta \approx 1.26 \). This value is low given the similarity of the process to the pore-force driven case. One explanation for this is the increased local friction due to chaperones binding in the vicinity of the pore on the trans side [33].

Under the ATA binding the polymer conformation on the trans side is very dense and accordingly motion of the monomers in it is highly correlated. We found that although tension propagation on the cis side is strong due to rapid translocation contribution of the trans side dominates the dynamics. We derived the scaling exponent \( \beta = 4/3 \) for the approximated case of a completely correlated moving (and growing) spherical polymer conformation on the trans side under constant bias translocation. This is very close to the value \( \beta \approx 1.36 \) obtained from our simulations.

To summarize, chaperone-assisted translocation of flexible polymers in three dimensions is highly dependent on the binding mechanism. Clear similarity to translocation driven by constant pore force was found for the single-binding scenario, whereas allowing binding to take place on multiple sites simultaneously changed the picture dramatically. The results presented here will pave the way for detailed understanding and possibly application of the many variations of chaperone-assisted biopolymer translocation.

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