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Electric Truck Hydropower, a flexible solution to hydropower in mountainous regions

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ABSTRACT

The world is undergoing a transition to a more sustainable energy sector dominated by renewable energy sources. This paper proposes an innovative solution that consists of catching water from streams at high altitudes to fill storage containers and transport them down a mountain, converting the potential energy of water into electricity with the regenerative braking systems of electric trucks and storing it in the truck's battery. The energy stored in the electric truck can be sold to the grid or used by the truck to transport other goods. Results show that the levelized cost of the electricity truck hydropower is 30–100 USD/MWh, which is cheap when compared with conventional hydropower 50–200 USD/MWh. The electricity generation world potential for the technology is estimated to be 1.2 PWh per year, which is equivalent to around 4% of the global energy consumption in 2019. Apart from being a low cost and impact electricity generation technology, electric truck hydropower can operate in combination with solar and wind resources and provide energy storage services to the grid.

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1. Introduction

Hydropower has seen continuous innovation for more than a century. For instance, Francis turbines are undergoing several innovations in their control and operation (X-blade, self-aeration, draft tube injection) [1]. Kaplan turbines have seen evolutions in more fish friendly turbines [2]. A lot of novel low head hydropower converters have been introduced. Also new approaches for the modernization of existing plants, such as dam heightening [3], new

electrical equipment, digitalization [4] and floating PV [5].

Currently, hydropower is limited to systems with two set water levels connected via canals, tunnels, and penstocks, and a turbine generation system converts the potential energy of the water into electricity (Fig. 1). In order to guarantee a large installed capacity and capacity factors higher than 30–40%, the catchment area must be high. This significantly reduces the potential of the technology in steep mountainous regions [6]. Additionally, storage reservoirs might also be required to regulate the flow of the river [7] to increase the capacity factor and economic viability of the plant. Furthermore, projected climate change scenarios indicate significant variation in hydropower potential with different regions alternately experiencing decrease and increase in potential [8–12].

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Fig. 1. Conventional hydropower in steep mountains. Kaprun hydropower and pumped storage plant in Austria. The plant consists of high dams and tunnels to increase the catchment area of the plant and to connect to the Salzach River and the lower reservoir Zeller See.

This further adds to financial uncertainty of projects. Despite the above mentioned complexity of hydropower development its role in the power system remains crucial [13] and is an established facilitator for the multipurpose uses of water, such as flood and drought mitigation, water storage, fishery, leisure, and for variable renewable energy sources' integration to the grid, as shown for example in the case study of West Africa [14]. Furthermore, in multiple studies the hydropower with reservoir became a foundation for solar-hydro [15,16], wind-hydro [6,17] and wind-solar-hydro [18] complementary operation.

In steep mountainous regions, the potential energy from a small water stream is high due to the large generation heads available. However, the catchment area for these streams is small, which results in a highly variable river flow [19], additionally highly susceptible to climate change [20] implying that a conventional hydropower plant would have low capacity factor and generation capacities, which would not guarantee a return for the investment.

In such cases, this paper proposes the use of Electric Truck Hydropower as an alternative to conventional hydropower.

2. Electric truck hydropower (ETH)

We propose a more flexible alternative for hydropower that features electric trucks. The proposed system consists of using existing road infrastructure that crosses mountain ranges to transport water down the mountain in electricity truck containers, transform the potential energy of the water into electricity with the regenerative braking of the truck and use this electricity to charge the battery of the truck. The ideal configuration of the ETH system is in mountainous regions with steep roads, where the same electrical trucks can be used to generate hydropower from different sites. This increases the chances that there will be water available to generate hydropower and thus increases the capacity factor of the system. Another benefit of the system is that only a small barrier is

required to abstract water from the river, there is no requirement for reservoirs to regulate the flow of the river. The reservoirs of this system are containers parked close to a river stream on the mountain, which are filled up with water extracted from the river. After the container is filled up, it is ready to be transported down the mountain and to generate hydropower. When the truck reaches the base of the mountain range, the container is parked close to the river, and the water in the container is slowly returned to the river to minimise the impact on the aquatic life. A similar case to ETH happens in the mining industry in Poland, where the extracted minerals are transported down a mountain with electric trucks, and each truck can generate up to 200 kWh per day [21].

The proposed system is divided into four main components, which are: the electric truck, water containers, the charge site and the discharge site, as shown in Fig. 2a. 1) The electric trucks have two main objectives, one of which is to transport water from the charged sites on the mountain to the discharge site. The other is to generate electricity by controlling the descending speed of the truck full of water, charging the battery in the truck. 2) The containers are used to continuously store water from the river in batches on the top of the mountain. It also continuously empties the water back to the river at the discharge site. It is important that the water extraction and release be continuous to reduce the

impact of the system on the river flow. 3) The charge sites are the locations where water is extracted from the river and introduced to the containers. They are located in the upper part of the mountain range, on tributary rivers, and/or intermediate locations, to increase the flexibility of the system. The electric truck enters the charge site with an empty container, leaves it to be filled with water, picks a container filled with water, and drives down the mountain. In cold regions, the charge sites on the top of the mountain might not be utilized, as the water in the river might freeze, and icy roads reduce the grip on the tires on the road and the efficiency of the system. 4) The discharge site is where water is removed from the truck and returned to the river. The electric truck enters the discharge site with a container full of water, leaves it to be emptied, collects an empty container, and drives up the mountain. The charged battery is replaced by a discharged battery. The battery is not fully discharged, as the truck requires energy to drive up the mountain with an empty container. The discharge site should have a robust connection to the national grid to allow the site to supply electricity to the grid [22]. During periods with low river flow, the battery packs will stop feeding electricity to the grid and will operate as a grid energy storage solution. Alternatively, the electric trucks can be used to transport goods.

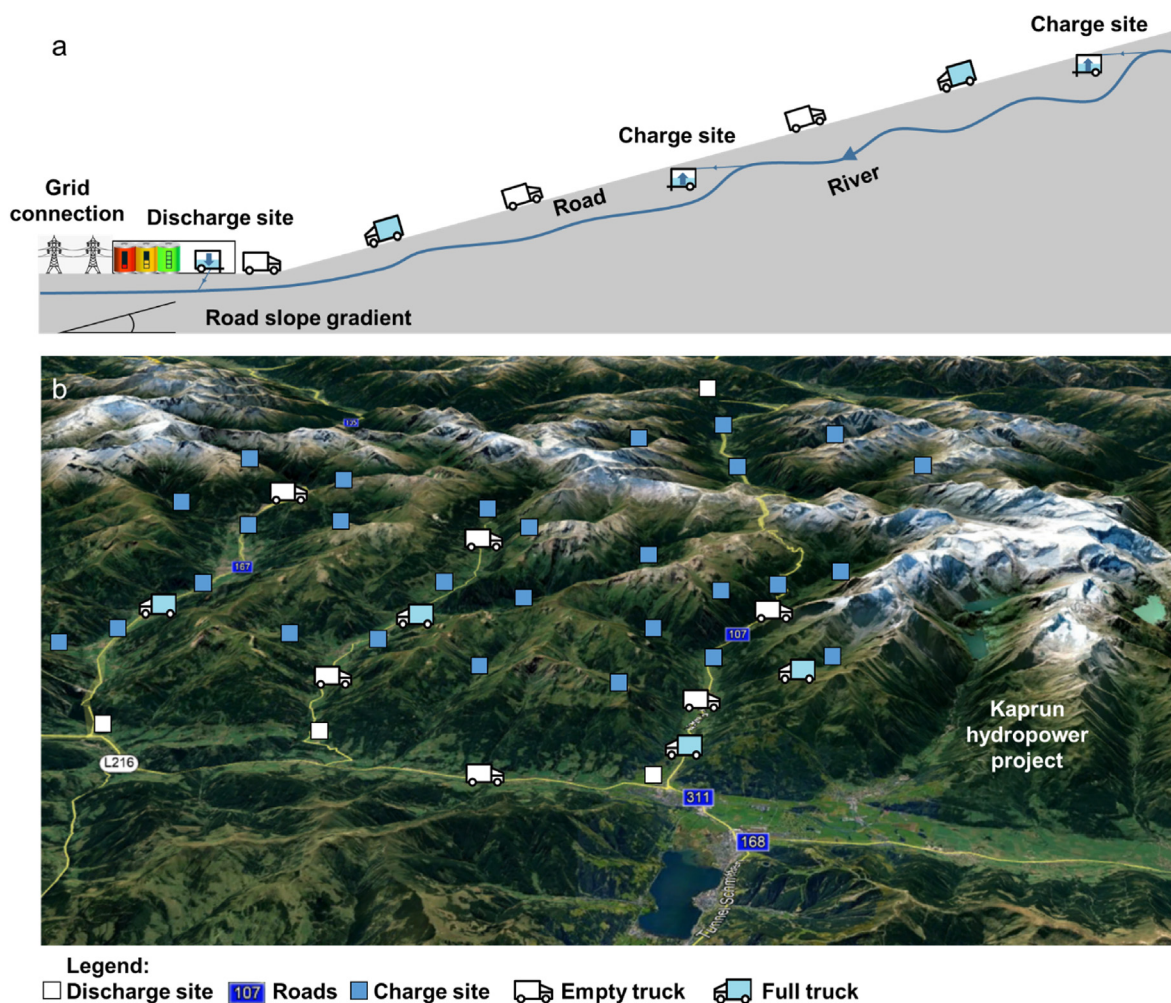


Fig. 2. Electric truck hydropower system. (a) axial description of the system where the empty truck moves up the mountain to collect the containers filled with water, and the truck with the full container goes down the mountain generating electricity. (b) aerial view of the ETH system compared with an existing hydropower project, highlighting the flexibility of ETH systems.

3. Methodology

The methodological framework used to estimate the global potential for hydropower electric trucks in this paper is described in Fig. 3. Each step of the methodology is detailed in the subsections below and highlighted in *italics* to facilitate the comprehension of the methodology description.

Step 1: ETH energy efficiency estimation. The *Electric truck description* applied in this paper is presented in Table 1. The proposed electric truck in this case study is taken from Ref. [23]. The costs and potential for ETH, as estimated in this paper applies to-day's electric truck costs. Note that these costs are expected to reduce significantly in the future. Given that the truck has the flexibility to move to mountains where it is raining or water is melting, the truck will operate at 70% capacity. Half of the time, the truck is moving up the mountain and the other half moving down the mountain, thus, the assumed generation capacity factor of an electric truck is 35%.

The theory behind the electricity truck hydropower concept can be derived from Eqs. (1)–(3). Eq. (1) shows the electric truck hydropower potential (*ETH* in J). Eq. (2) calculates the potential energy that can be extracted from the system (*E* in J), and Eq. (3) calculates the energy losses in the truck, which is mainly related to the *rolling resistance losses* of the tires and the aerodynamic friction *drag losses* in the truck (*L* in J).

$$ETH = E - L \quad (1)$$

$$E = m \times h \times g \times b \times M \quad (2)$$

where *E* is the potential energy of the system (in J), *m* is the mass of water added to the container in the upper water catchment location (in kg), *h* is the altitude difference between the charge site and the discharge site (in m), *g* is the acceleration of gravity and equal to 9.81 m/s², and *b* is the battery's energy storage efficiency cycle, assumed to be 90%. *M* is the efficiency of electric motor and

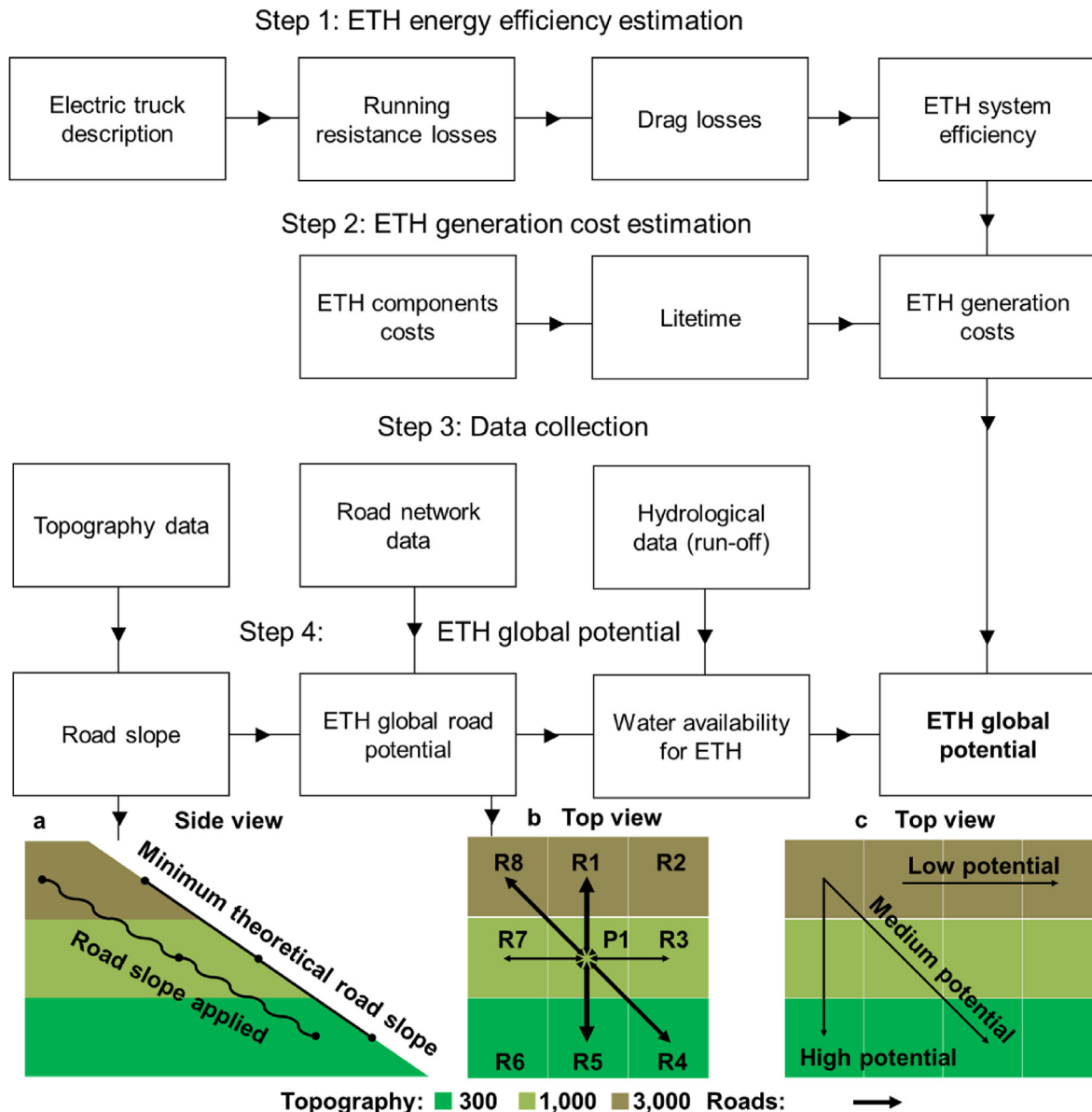


Fig. 3. Methodology to calculate the ETH global potential.

Table 1
Electric truck description [23].

Item	Description
Manufacturer	Ningbo Berzon Hida Trading Co.
Reference	[23]
Truck and battery cost (USD)	145,000 USD
NEDC Max. Range (km)	500
Range fully loaded and 40 km/h (km)	200
Battery warranty (km)	80,000
Dimensions (m)	L 6500 x W 2500 x H 3600
Economic speed (km/h)	30–50
Total traction mass (kg)	33,100
Battery weight (kg)	1000
Curb weight (kg)	9930
Water capacity (kg)	23,170
Battery capacity (kWh)	250
Motor type	Permanent magnet synchronous motor
Drive motor rated power (KW)	250
Drive motor rated speed (r/min)	1195
Drive motor rated torque (N.M)	2000
Drive motor peak power (KW)	350
Drive motor peak speed (r/min)	3400
Drive motor peak torque (N.M)	3500
Rolling resistance coefficient	0.01
Drag coefficient	0.36
Truck frontal area (m ²)	9.13
Front axle bearing (tons)	6.5
Rear axle bearing (tons)	11.5
Rear axle ratio	4.1
Interest rate (%)	4.0

transmission system, assumed to be 90% [24].

$$L = \frac{\mu \times w \times g + 0.5C_D \times \rho \times A \times V^2}{s} \times h \quad (3)$$

where, μ is the rolling resistance coefficient, between the tires and road, assumed to be 0.01 [25]. w is the mass of the truck with or without water, moving down and up a mountain respectively (in kg). The empty truck goes up the mountain with 9930 kg, but it goes down the mountain filled with water with 33,100 kg. In other words, the truck weight going up is 30% of the weight of the truck going down. C_D is the drag coefficient, assumed to be 0.36 [26], ρ is the air density, assumed to be 1.275 kg/m³. A is the frontal area of the truck (in m²). V is the velocity of the truck (in m/s). s is the road slope gradient (in %); for example, a slope gradient of 15% means a 1 m vertical and 6.7 m horizontal distance. The slope gradient is high because the system is designed to operate on existing steep roads. Note that Equation (3) assumes that the mountain roads are smooth.

Step 2: ETH generation cost estimation. The main costs parameters are described in Table 1 (*ETH component costs*). The assumed capacity factor for the trucks is 35% (assuming that half of the time the trucks are moving up the mountains, the capacity factor of the trucks is 70%). The *Lifetime* of the trucks is assumed to be limited to the mileage of the truck, which is 1,600,000 km. This results in a lifetime of 6.5 if it operates at a speed of 40 km/h. Given that the truck is expected to operate for 7 years, the lifetime of the battery is assumed to be the same as the truck. The global estimate for *ETH generation costs* is set for a range of velocities and road slope gradients. For each available road slope, the truck velocity that results in the minimum generation cost is selected.

Step 3: Data collection. The data applied in the methodology to estimate the global potential for ETH are global topographic, road network and hydrological (run-off). This data is detailed in Table 2. The topographic data used is the Shuttle Radar Topography Mission (SRTM) developed by NASA [27]. It has a 3 arc seconds (~90 × 90 m) resolution. The average altitude is used to reduce the resolution to 5

arc minutes resolution (~8 × 8km) to compare with the available road infrastructure data. This data is used to find the altitude difference between two connected locations and to estimate the road slope. The road infrastructure data used is the Global Roads Inventory Project (GRIP) developed by GLOBIO [28]. The unit of the data is the total road density in m/km². This unit is transformed into a road index by applying a logarithm with a base of 10. The run-off data used is the ERA5 developed by ECMWF [29]. The data consists of land monthly average run-off data from 1981 to the present, the exact data entered in the website is ("Monthly average reanalysis", "2020", "January" to "December", "Surface runoff", "Whole available region" and "NetCDF").

Step 4: ETH global potential. There are three main limitations to the potential for ETH. The first and most important is the change in topography, which is described in Fig. 3 and is used to estimate the *road slope*. By combining the road slope with the existing road infrastructure, one can estimate the *ETH global road potential*. Then the *water availability for ETH* can restrict the road potential and the existing amount of water available for hydropower. The equation applied to estimate the ETH global potential is described in Eq. (5). The potential for ETH is estimated in a resolution of 5 arc minutes (~8 × 8km). To better present the results the ETH potential in a 1-degree resolution is summed.

$$P = \sum_{i=1}^n G_i(S_i(\frac{\Delta H_i}{D_i}), R_i, W_i) \quad \text{if } C(S(\frac{\Delta H_i}{D_i})) < 200 \quad (5)$$

where P is the ETH generation potential for the point under analysis (PUA) in a 5 min resolution (in GWh), i is one combination between the PUA and a point surrounding it (PSI), n is the number of PSI surrounding PUA, which is equal to 8 (Fig. 3 b). G is the ETH generation potential of each road segment in GWh per year and is a function of S , R and H . S is the road slope applied, which is a function of the minimum theoretical road slope. This equation was created comparing the real road slope of existing roads in different countries with different observed minimum theoretical road

Table 2
Data input to the model.

Data	Available resolution	Applied resolution	Reference
Topography (SRTM)	3 arc seconds ($\sim 90 \times 90$ m)	5 arc minutes ($\sim 8 \times 8$ km)	[27]
Road infrastructure (GRIP)	5 arc minutes ($\sim 8 \times 8$ km)	5 arc minutes ($\sim 8 \times 8$ km)	[28]
Run-off data (ECMWF)	6 arc minutes ($\sim 10 \times 10$ km)	5 arc minutes ($\sim 8 \times 8$ km)	[29]

slopes. ΔH is the minimum height difference between PUA and PSI. D is the horizontal distance between PUA and PSI. At the equator, the distance is equal to 8 km, and it decreases with the change in latitude away from the equator. The total distance travelled by the truck is equal to D divided by the slope. R is the road infrastructure connecting PUA and PSI. It consists of the logarithm in the tenth base of the data from GRIP in m/km^2 and varies from ~ 0 to 5. The impact of each element of the road infrastructure on the ETH potential is shown in Table 3. The traffic in the mountain roads and the O&M of the roads that are continuously used by heavy trucks are not included in the cost analysis. W is the annual average superficial run-off in the PSI, which limits the potential for ETH according to the water available to be used for hydropower, as shown in Table 3. The amount of water assumed to estimate the potential for hydropower is 10% of the surface flow in the rivers. This is a small amount that does not have a large impact on the aquatic life or the river but still allows the trucks to maintain a large generation capacity of the system. The time required to fill the container with water will depend on the river flowrate and the number of trucks moving up and down the mountain. Assuming a storage capacity of 23 m^3 and a flowrate of $0.1 \text{ m}^3/\text{s}$, it takes 4 min to fill up the container. The potential for ETH is only considered if the levelized cost of electricity (C), which are a function of the road slope applied, are lower than 200 USD/MWh.

4. Results

Applying the methodology described in the methods section and Fig. 3 and using data on topography [27], hydrological run-off [29], and road infrastructure [28] (Fig. 4a,b, c and Table 2), the results presented in Fig. 4 were found. The topographic data is used to estimate the minimum theoretical road slope. To consider road curves, the function in Fig. 4d is applied to find the road slope applied. A limit of 15% road slope was found in the analysis of the road aiming to cross steep mountains. This limit is applied due to high road maintenance costs, limits in the truck capacity to carry a load, and due to icy roads in high mountains or cold locations. As the minimum theoretical road slope in the topographical data with 5 min resolution does not surpass 20%, the maximum road slope gradient applied to estimate the global potential for ETH is 12%, as shown in Fig. 4f. The most important parameter that impacts both the efficiency and levelized cost of generation in ETH systems is the road slope gradient of the road (Fig. 4e,g). The efficiency of the ETH system varies from 68% with a road slope of 15% and a speed of 40 km/h, to 35% with a road slope of 5% and speed of 60 km/h

(Fig. 4e). As shown in Fig. 4h, the minimum levelized cost of ETH is 30 USD/MWh and is focused on steep mountains. The estimated potential of ETH is presented in Fig. 4i. It shows that some locations in the Andes and the Himalayas have the potential to generate 15 TWh per year in a 1-degree resolution. Fig. 4j presents the potential for ETH divided into seven different continents in cost curves, assuming a generation cost lower than 100 USD/MWh. The continent with the highest potential is Asia with 617 TWh, South America with 466 TWh, Central America with 65 TWh, Europe with 56 TWh, Africa with 17 TWh, North America with 5 TWh, and Australia with 0.7 TWh. The global potential for ETH is estimated to be 1226 TWh.

Table 4 presents the ETH levelized cost of generation in USD/MWh. The truck speed that results in the lower ETH levelized cost varies with each road slope. The levelized cost applied in the paper are the ones highlighted in green. The occasions where the slope is high and electric trucks would not have the power or breaking capacity to drive at high speeds up and down a mountain are highlighted in red. Table 3 presents the road limits and assumptions used in the model. It assumes that the roads are also used for other purposes and the potential use of the road for ETH is limited to the velocity, number of trucks per hour and water availability.

5. Discussion

This system considers that the weight of the empty truck is 30% of the truck filled with water, with its equivalent to the specification of the truck used as the basis for this study [23]. Accordingly, reducing the curb weight of the truck could significantly increase the efficiency of the system and lower the generation costs. Alternatives to reduce the weight of the truck include using aluminium or carbon fibre instead of steel. With trucks being operated autonomously in the future, they could be built without the front section, which could further reduce the curb weight of the truck and the efficiency of ETH systems. The energy storage capacity of the battery should be similar to the amount of energy generated with the ETH system, with the intent of minimising the weight of the truck's battery pack. Another optimized option to further reduce the weight of the truck is to use composite structural batteries (e.g., using modified carbon fibres) which increase the recharge mileage and have potential to substantially to reduce the weight of electric-powered systems [40,41]. This study assumes that the electric truck is autonomous, which significantly reduces the fixed costs of the system.

With the intent of increasing the applicability and viability of

Table 3
Road limits and assumptions used in the model.

Road index	Maximum Velocity (m/s)	Road description	Number of trucks per hour	Water flow (m^3/s)	Road slope (%) and ETH generation (GWh per year)					
					2.5	5	7.5	10	12.5	15
1	40	One lane, unpaved	200	1.8	2.5	47.3	92.1	136.9	181.8	327.0
2	60	One lane, paved	300	2.8	3.8	71.0	138.2	205.4	272.6	490.5
3	60	Two lanes, paved	600	5.5	7.6	142.0	276.4	410.8	545.3	980.9
4	60	Three lanes, paved	900	8.3	11.5	213.1	414.7	616.3	817.9	1471.4
5	60	Four lanes, paved	1200	11.0	15.3	284.1	552.9	821.7	1090.5	1961.8

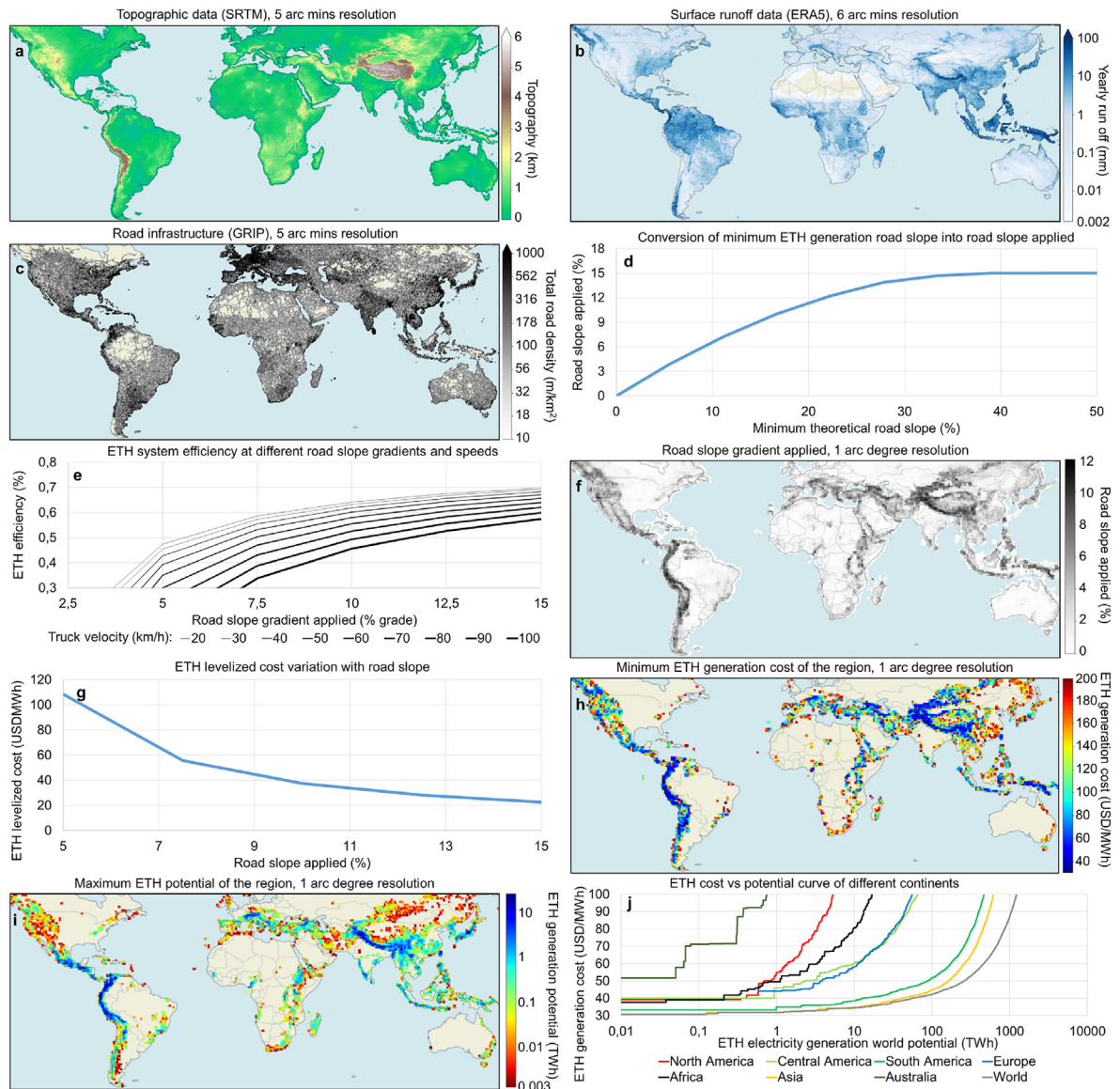


Fig. 4. World potential for electric truck hydropower. (a) Topographic data (SRTM), 5 arc mins resolution. (b) Surface runoff data (ERA5), 6 arc mins resolution. (c) Road infrastructure (GRIP), 5 arc mins resolution. (d) Conversion of minimum ETH generation road slope into road slope applied. (e) ETH system efficiency at different road slope gradients and speeds. (f) Road slope gradient applied in a 1 arc degree resolution. (g) ETH leveled cost with road slope. (h) Minimum ETH generation costs of the region, 1 arc degree resolution. (i) Maximum ETH potential of the region, 1 arc degree resolution. (j) ETH cost vs potential curve of different continents.

Table 4

ETH leveled cost of generation in USD/MWh.

Road slope	Trucks speed (km/h)			
	20	40	60	80
5	110.4	108.5	127.2	180.3
7.5	59.5	55.8	59.0	67.5
10	40.8	37.5	38.4	41.5
12.5	31.0	28.3	28.5	30.0
15	25.0	22.7	22.6	23.4
17.5	21.0	18.9	18.8	19.3
20	18.0	16.3	16.0	16.3
22.5	15.8	14.2	14.0	14.2
25	14.1	12.7	12.4	12.5

the electricity truck hydropower, the trucks could be built with a water tank that varies in volume according to the truckload (Fig. 5 a b). For example, if the truck volume is only half loaded, the other half of the truck cargo volume could be filled with water on the top of a mountain to charge the battery of the truck on the way down. When the truck reaches the bottom of the mountain, it will then empty the water in a discharge station and continue driving with the cargo, but without water. Apart from generating hydropower, the water input to the truck could be cooled or heated up before being added to the truck to provide cooling or heating services to the load. Being thereby a multipurpose facility as it can be for example realized for seawater used both for fresh water provision (through desalination) and cooling [39]. In the case of cooling services, the truck could also be filled with ice slurry, which would contribute to a higher cooling capacity due to the phase change of water. Note that the introduction of ice slurry is not appropriate for locations with temperatures below 0 °C, because the ice slurry

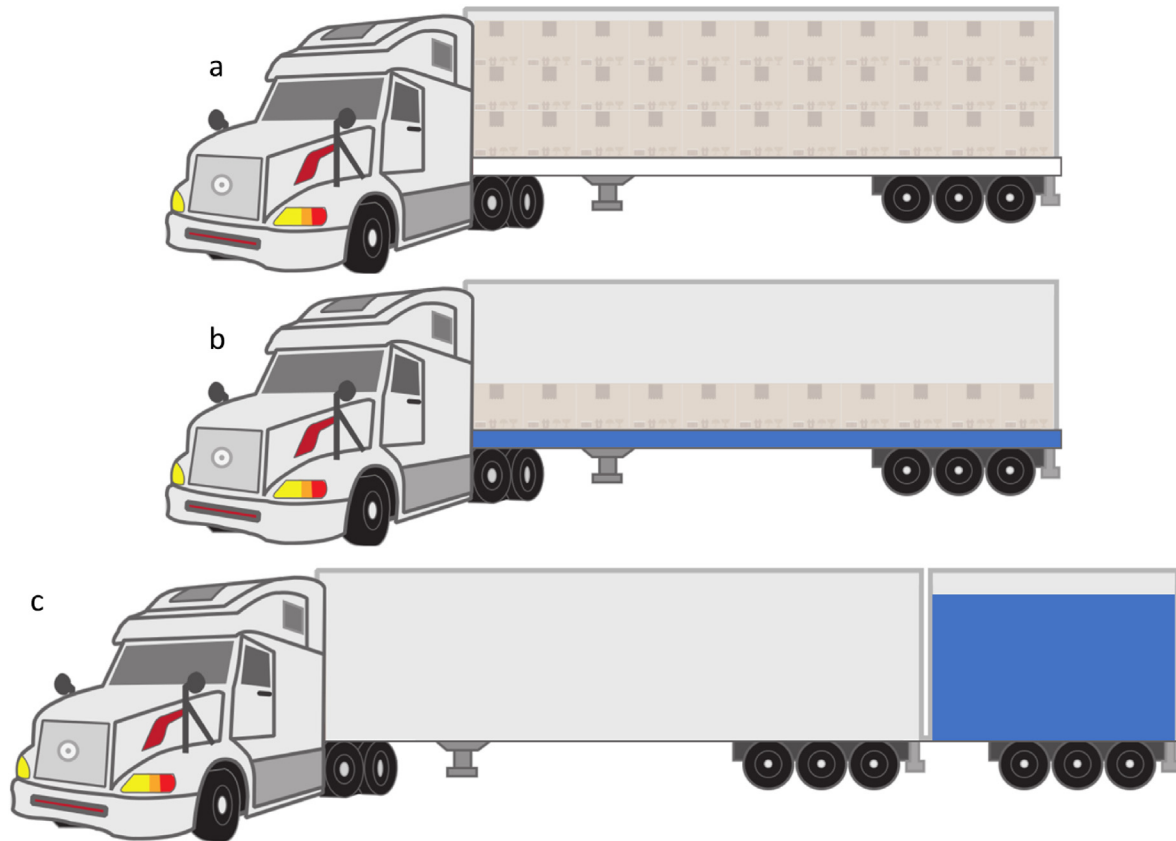


Fig. 5. Hybrid cargo, hydropower truck. (a) fully loaded with cargo and empty water tank. (b) cargo and water tank partly loaded. (c) empty cargo and fully loaded tank.

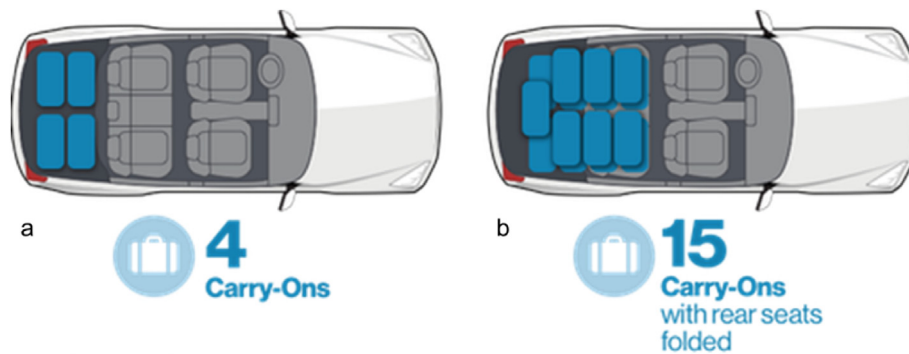


Fig. 6. Number of cases that fit in an electric car. (a) with rear seats unfolded, (b) with rear seats folded [38].

would freeze, which would make it difficult to unload the water when the tank reaches the bottom of the mountain. Another option is to connect another wagon to the truck filled with water (Fig. 5 c).

Recently developed electric vehicles can store four to six cases with rear seats unfolded, and 14 to 16 cases with rear seats folded [38], as shown in Fig. 6 a,b. The dimensions of the cases are 55 cm × 35 cm × 22 cm and weigh 42 kg each when full of water. Table 5 presents the amount of energy that can be regenerated with an electricity car full of water. It assumes that 60% of the energy that would be wasted to control the speed of the electric car going down a 2000 m mountain and is turned into electricity to charge the battery of the car. Assuming the car has a battery charge of 50 kWh, the car without water will charge around 10% of its battery. If the car has an additional 677 kg of water, it will charge 15% of its

Table 5

Electric vehicle with and without suitcases.

Car arrangement	Car weight (kg)	Car charge (%)
Without water	1611	10.53594
With 6 suitcases with water	1865	12.19775
With 16 suitcases with water	2289	14.96744

battery. This charge difference is not substantial, mainly because cars have a limited volume to store water.

Apart from providing hydropower, the system can also provide cooling and water delivery services to customers below the mountain. Table 6 presents the difference in energy potential for

Table 6
Hybrid hydropower and cooling electricity truck potential compared to the cooling services.

ETH generation head (m)	Hydropower (Wh/kg)	Cooling with hydropower ^a (Wh/kg)	Cooling with ice (Wh/kg)	Share of cooling energy compared with hydropower (%)
6000	13.08	52.3	92.8	56.4
5000	10.9	43.6	92.8	47.0
4000	8.72	34.9	92.8	37.6
3000	6.54	26.2	92.8	28.2
2000	4.36	17.4	92.8	18.8
1000	2.18	8.7	92.8	9.4

^a Assuming a refrigeration system with a COP of 4.

Table 7
Comparison between electric truck hydropower generation and conventional hydropower.

Characteristic	Conventional hydropower	Electric truck hydropower
Location flexibility	Low: The plant will always operate in the same location.	High: The trucks can move to different mountains according to water availability.
Head flexibility	Low: The altitude at which the water enters and leaves the system is fixed	High: The head where the water is caught varies in different seasons or with weather events.
Capacity factor	50%: The plant is designed to have a certain capacity factor, but there are limited mountains that can guarantee a high-capacity factor. Water wheels, Archimedes screw and small Pelton turbines are examples of flexible turbines that can handle variable flows.	35%: Given the need to move up and down, the truck is not available at all times in generation mode.
Generation Efficiency	90%: The efficiency of conventional hydropower plants is very high.	30–60%: The efficiency of electric truck hydropower varies with the driving speed and the road slopes, and is shown in Fig. 4e.
Storage reservoirs	Required to regulate the river flow and increase the capacity factor of the system. Typically, in high mountains there are waterfalls, so fish migration problem does not exist naturally, and small barriers are generally built-in the proximity of these falls, and also serve as hydraulic structures to stabilize the river bed,	Not required as the trucks can move to where it is raining, or ice is melting. ETH can only replace very small hydropower plants. Hydropower plants in high mountains are generally installed to satisfy peak demand energy request.
Seasonal storage	Hydropower and pumped hydropower storage reservoirs can provide seasonal energy and water storage [30–34].	Electricity truck hydropower does not provide seasonal storage, due to its limited storage capacity. Other technologies could complement its lack of seasonal storage [35–37].
Applicability	Large rivers with high catchment areas	Small rivers with small catchment areas.
Modularity	Not modular. Each project is different from the other. The larger the volume of water, the lower the costs.	Modular. The generation capacity depends on the number of electric trucks in the system. This is particularly interesting in isolated areas where the demand for electricity is small.
Multipurpose	Yes. Conventional hydropower also provides water storage, flood and drought mitigation, fishery and leisure	Yes. Apart from generating energy, the trucks can supply water and cooling services.
Lifetime	40–100 years	3–10 years
CAPEX	High (1000–5000 USD/kW)	Low (200–500 USD/kW)
OPEX	Low (5% of investment costs per year)	Medium (15% of investment costs per year)
Levelized cost	50–200 USD/MWh	30–100 USD/MWh

electric truck hydropower and cooling potential at different generation heights. The hybrid hydropower and cooling electric truck arrangement can be designed to store cooling energy from the top of a mountain on weekly, monthly, or seasonal scales. The seasonal scale is the one with the highest potential, which stores cold temperatures during the winter and uses it during the summer. An interesting case study for this is to freeze water in containers in the mountains surrounding the city of Phoenix, Arizona, and during the summer use the ice for cooling in the city.

Table 7 presents a comparison of different aspects between electric truck hydropower generation and conventional hydropower.

6. Conclusions

It is difficult to harness the hydropower potential of a mountain with conventional technologies because of their rigid structure, high investment costs (particularly for small capacity projects), operational and head inflexibility, and the need for storage reservoirs and non-modularity (Table 7). Even though conventional hydropower systems have long lifetimes (40–100 years) and ETH projects have short ones (3–10), the CAPEX and levelized costs of conventional hydropower projects (1000–5000 USD/kW and 50–200 USD/MWh) are higher than for ETH projects (200–500

USD/kW and 30–100 USD/MWh). Given that the ETH system is already a competitive electricity generation alternative with existing technology, its cost is expected to further reduce [42] with expected technological improvements in the near future. Results show that the lower the truck speed, the fewer are the energy losses, but the least electricity is generated per year. The greater the speed, the greater are the losses, but the generation is greater per year. As the ETH system should achieve a short payback time, the speed of the truck should be as high as possible to maximise the returns in the investment.

Mountain regions are characterised by high precipitation, as the high mountain relief results in strong upward air flows, cooling the air and condensing moisture from it as rain or snow. Given the rocky soil characteristics of mountain areas, little of this water is absorbed. Thus, where the precipitation falls in liquid form, there is high surface run-off directly to river. River flows will be especially high in springtime when melting of precipitation stored in frozen form over winter occurs. To the best of our knowledge, this is the first occasion that a flexible low-carbon hydropower-generation system of low technology complexity integrating electrical trucks is examined. It is possible to derive from our study future opportunities to integrate the proposed system with PV and wind energy systems [43], contributing with the decarbonisation of power generation.

Data availability

The spreadsheet with efficiency and economic calculations and the global potential for ETH model applied in the paper can be downloaded from <https://github.com/JulianHunt4/Electric-Truck-Hydropower>.

Credit author statement

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Conceptualization, J.H., J.J.; methodology, B.Z., A.N.; formal analysis, S.C.; investigation, C.C.; data curation, D.P.; writing—original draft preparation, J.H.; writing—review and editing, B.Z.; visualization, P.P.; project administration, W.F., B.R.; funding acquisition, A.N.; resources, F.T.; software, R.S. All authors have read and agreed to the published version of the manuscript.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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References

- [1] Sari MA, Badruzzaman M, Cherchi C, Swindle M, Ajami N, Jacangelo JG. Recent innovations and trends in in-conduit hydropower technologies and their applications in water distribution systems. *J Environ Manag* 2018;228:416–28. <https://doi.org/10.1016/j.jenvman.2018.08.078>.
- [2] Kougias I, Aggidis G, Avellan F, Deniz S, Lundin U, Moro A, et al. Analysis of emerging technologies in the hydropower sector. *Renew Sustain Energy Rev* 2019;113:109257. <https://doi.org/10.1016/j.rser.2019.109257>.
- [3] Hunt JD, Byers E, Prenner R, Freitas MAV de. Dams with head increaser effect: harnessing potential and kinetic power from rivers with large head and flow variation. *Energy Convers Manag* 2018. <https://doi.org/10.1016/j.enconman.2017.12.034>.
- [4] Quaranta E, Aggidis G, Boes RM, Comoglio C, De Michele C, Ritesh Patro E, et al. Assessing the energy potential of modernizing the European hydropower fleet. *Energy Convers Manag* 2021;246:114655. <https://doi.org/10.1016/j.enconman.2021.114655>.
- [5] Silvério NM, Barros RM, Tiago Filho GL, Redón-Santafé M, Santos IFS dos, Valério VE de M. Use of floating PV plants for coordinated operation with hydropower plants: case study of the hydroelectric plants of the São Francisco River basin. *Energy Convers Manag* 2018;171:339–49. <https://doi.org/10.1016/j.enconman.2018.05.095>.
- [6] Hunt JD, Falchetta G, Parkinson S, Vinca A, Zakeri B, Byers E, et al. Hydropower and seasonal pumped hydropower storage in the Indus basin: pros and cons. *J Energy Storage* 2021;41:102916. <https://doi.org/10.1016/j.est.2021.102916>.
- [7] Little JDC. The use of storage water in a hydroelectric system. *J Oper Res Soc Am* 1955;3:187–97. <https://doi.org/10.1287/opre.3.2.187>.
- [8] Turner S, Hejazi M, Kim S, Clarke L, Edmonds J. Climate impacts on hydropower and consequences for electricity supply investment needs. *Energy* 2017;141. <https://doi.org/10.1016/j.energy.2017.11.089>.
- [9] Tariku TB, Gan KE, Tan X, Gan TY, Shi H, Tilmant A. Global warming impact to River Basin of Blue Nile and the optimum operation of its multi-reservoir system for hydropower production and irrigation. *Sci Total Environ* 2021;767:144863. <https://doi.org/10.1016/j.scitotenv.2020.144863>.
- [10] Maran S, Volonterio M, Gaudard L. Climate change impacts on hydropower in an alpine catchment. *Environ Sci Pol* 2014;43:15–25. <https://doi.org/10.1016/j.envsci.2013.12.001>.
- [11] Hunt JD, Nascimento A, Caten CS ten, Tomé FMC, Schneider PS, Thomazoni ALR, et al. Energy crisis in Brazil: impact of hydropower reservoir level on the river flow. *Energy* 2022;239:121927. <https://doi.org/10.1016/j.energy.2021.121927>.
- [12] Hunt JD, Leal Filho W. Land, Water, and Wind Watershed Cycle: a strategic use of water, land and wind for climate change adaptation. *Clim Change* 2018;147:427–39. <https://doi.org/10.1007/s10584-018-2164-8>.
- [13] Hydropower IEA. Has a crucial role in accelerating clean energy transitions to achieve countries' climate ambitions securely. IEA; 2021. <https://www.iea.org/news/hydropower-has-a-crucial-role-in-accelerating-clean-energy-transitions-to-achieve-countries-climate-ambitions-securely>.
- [14] Sterl S, Vanderkelen I, Chawanda CJ, Russo D, Brecha RJ, van Griensven A, et al. Smart renewable electricity portfolios in West Africa. *Nat Sustain* 2020;3:710–9. <https://doi.org/10.1038/s41893-020-0539-0>.
- [15] Fang W, Huang Q, Huang S, Yang J, Meng E, Li Y. Optimal sizing of utility-scale photovoltaic power generation complementarily operating with hydropower: a case study of the world's largest hydro-photovoltaic plant. *Energy Convers Manag* 2017;136:161–72. <https://doi.org/10.1016/j.enconman.2017.01.012>.
- [16] Hunt JD, Freitas MAVD, Pereira Junior AO. A review of seasonal pumped-storage combined with dams in cascade in Brazil. *Renew Sustain Energy Rev* 2017;70. <https://doi.org/10.1016/j.rser.2016.11.255>.
- [17] Levieux LI, Inthamoussou FA, De Battista H. Power dispatch assessment of a wind farm and a hydropower plant: a case study in Argentina. *Energy Convers Manag* 2019;180:391–400. <https://doi.org/10.1016/j.enconman.2018.10.101>.
- [18] Liu B, Lund JR, Liao S, Jin X, Liu L, Cheng C. Optimal power peak shaving using hydropower to complement wind and solar power uncertainty. *Energy Convers Manag* 2020;209:112628. <https://doi.org/10.1016/j.enconman.2020.112628>.
- [19] Pilgrim DH, Cordery I, Baron BC. Effects of catchment size on runoff relationships. *J Hydrol* 1982;58:205–21. [https://doi.org/10.1016/0022-1694\(82\)90035-X](https://doi.org/10.1016/0022-1694(82)90035-X).
- [20] Etter S, Addor N, Huss M, Finger D. Climate change impacts on future snow, ice and rain runoff in a Swiss mountain catchment using multi-dataset calibration. *J Hydrol Reg Stud* 2017;13:222–39. <https://doi.org/10.1016/j.jehrh.2017.08.005>.
- [21] Auto Świat. Największy pojazd elektryczny świata, który nie wymaga ładowania (eng. The largest electric vehicle in the world that does not need to be recharged). Auto-Świat; 2021. <https://cutt.ly/DPTkwsU>.
- [22] Borlaug B, Muratori M, Gilleran M, Woody D, Muston W, Canada T, et al. Heavy-duty truck electrification and the impacts of depot charging on electricity distribution systems. *Nat Energy* 2021;6:673–82. <https://doi.org/10.1038/s41560-021-00855-0>.
- [23] Ningbo Berzon Hida Trading Co. Very strong, beautiful electric tractor/truck with 90km/h and 200km range. Alibaba 2021. https://www.alibaba.com/product-detail/Very-strong-beautiful-electric-tractor-truck_60810629043.html?spm=a2700.galleryofferlist.normal_offer.d_image.32cd62f1DD5iLr.
- [24] Xiaozheng H. Eco-driving advisory strategies for a platoon of mixed gasoline and electric vehicles in a connected vehicle system. *Transport Res Part D Transp Environ* 2018;63:907–22.
- [25] Mao Y, Wen S, Chen Y, Zhang F, Panine P, Chan TW, et al. High performance graphene oxide based rubber composites. *Sci Rep* 2013;3:2508. <https://doi.org/10.1038/srep02508>.
- [26] Mohan A, Sripad S, Vaishnav P, Viswanathan V. Trade-offs between automation and light vehicle electrification. *Nat Energy* 2020;5:543–9. <https://doi.org/10.1038/s41560-020-0644-3>.
- [27] Information C-C for S. SRTM 90m digital elevation data. 2017.
- [28] Meijer JR, Huijbregts MAJ, Schotten KCGJ, Schipper AM. Global patterns of current and future road infrastructure. *Environ Res Lett* 2018;13:64006. <https://doi.org/10.1088/1748-9326/aab4d2>.
- [29] ECMWF. ERA5 – land monthly average data from 1981 to present. Copernicus; 2021. <https://cds.climate.copernicus.eu/cdsapp#!/dataset/reanalysis-era5-land-monthly-means?tab=form>.
- [30] Hunt JD, Zakeri B, Lopes R, Barbosa PSF, Nascimento A, Castro NJ de, et al. Existing and new arrangements of pumped-hydro storage plants. *Renew Sustain Energy Rev* 2020;129:109914.
- [31] Hunt J, Byers E, Wada Y, Parkinson S, Gernaat D, Langan S, et al. Global resource potential of seasonal pumped-storage for energy and water storage. *Nat Commun* 2020;11. Article number: 947.
- [32] Hunt J, Byers E, Riahi K, Langan S. Comparison between seasonal pumped-storage and conventional reservoir dams from the water, energy and land nexus perspective. *Energy Convers Manag* 2018;116:385–401.
- [33] Hunt JD, Stilpen D, de Freitas MAV. A review of the causes, impacts and solutions for electricity supply crises in Brazil. *Renew Sustain Energy Rev* 2018;88. <https://doi.org/10.1016/j.rser.2018.02.030>.
- [34] Hunt JD, Freitas MAV, Pereira Junior AO. Enhanced-Pumped-Storage: combining pumped-storage in a yearly storage cycle with dams in cascade in Brazil. *Energy* 2014;78. <https://doi.org/10.1016/j.energy.2014.10.038>.
- [35] Hunt JD, Zakeri B, Leal Filho W, Schneider PS, de Assis Brasil Weber N, Vieira LW, et al. Swimming pool thermal energy storage, an alternative for distributed cooling energy storage. *Energy Convers Manag* 2021;230:113796. <https://doi.org/10.1016/j.enconman.2020.113796>.
- [36] Hunt JD, Zakeri B, Falchetta G, Nascimento A, Wada Y, Riahi K. Mountain

- Gravity Energy Storage: a new solution for closing the gap between existing short- and long-term storage technologies. *Energy* 2020;190:116419. <https://doi.org/10.1016/j.energy.2019.116419>.
- [37] Hunt JD, Guillot V, Freitas MAV de, Solari RSE. Energy crop storage: an alternative to resolve the problem of unpredictable hydropower generation in Brazil. *Energy* 2016. <https://doi.org/10.1016/j.energy.2016.02.011>.
- [38] Capparella J. Tesla model 3 cargo space and storage. *Car Driv* 2018. <https://www.caranddriver.com/reviews/in-depth-review/a19755893/2018-tesla-model-3-cargo-space-storage/>; 2018.
- [39] Hunt JD, Weber N de AB, Zakeri B, Diaby AT, Byrne P, Filho WL, et al. Deep seawater cooling and desalination: combining seawater air conditioning and desalination. *Sustain Cities Soc* 2021;74. <https://doi.org/10.1016/j.scs.2021.103257>.
- [40] Hong Z, Hu Z, Yang R, You J, Fu Y, Zhou L, et al. Multiphysics modeling framework for composite structural batteries with modified carbon fibers as electrodes. *Compos Commun* 2021;27:100853. <https://doi.org/10.1016/j.coco.2021.100853>.
- [41] Chen J, Zhou Y, Islam MS, Cheng X, Brown SA, Han Z, et al. Carbon fiber reinforced Zn–MnO₂ structural composite batteries. *Compos Sci Technol* 2021;209:108787. <https://doi.org/10.1016/j.compscitech.2021.108787>.
- [42] Nykvist B, Nilsson M. Rapidly falling costs of battery packs for electric vehicles. *Nat Clim Change* 2015;5:329–32. <https://doi.org/10.1038/nclimate2564>.
- [43] Lu L, Yuan W, Su C, Wang P, Cheng C, Yan D, et al. Optimization model for the short-term joint operation of a grid-connected wind-photovoltaic-hydro hybrid energy system with cascade hydropower plants. *Energy Convers Manag* 2021;236:114055. <https://doi.org/10.1016/j.enconman.2021.114055>.